



The scroll compressor with internal cooling system – conception and CFD analysis

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Outline

- Motivation
- Vanes shape comparison
- Heat transfer in working chamber
- CFD simulation
 - assumptions
 - dynamic mesh
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- Summary

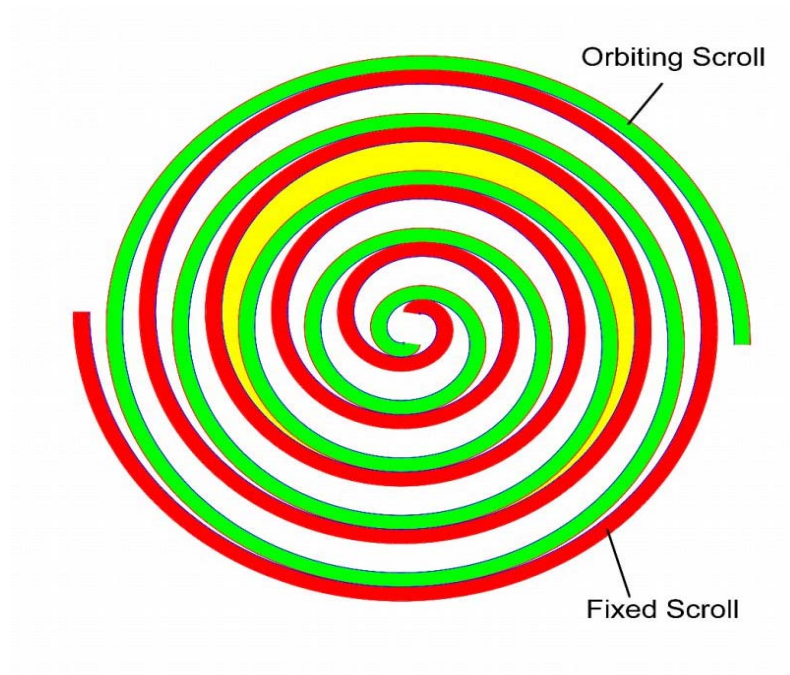


Motivation

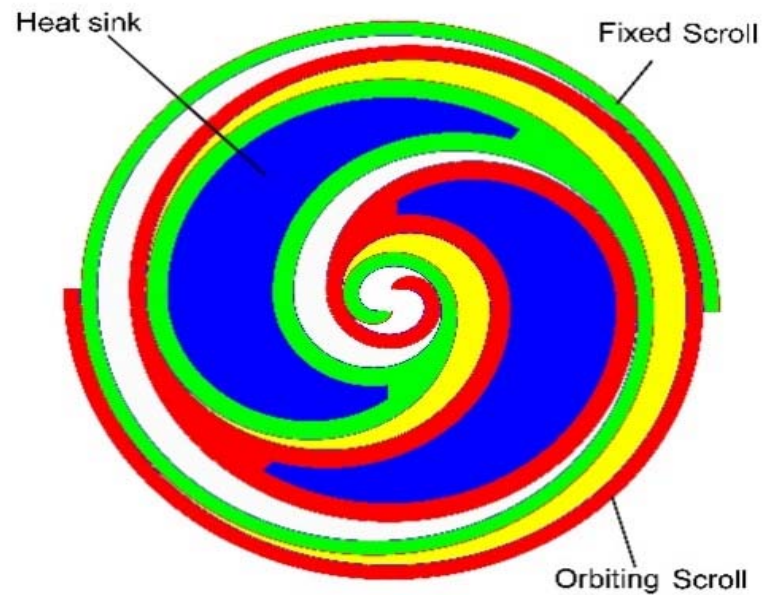
- Making the compression proces more effective
- Study of the modified shape
- Knowledge about a heat-flow phenomena
- Building a device for special applications



Vanes shape comparison



classic

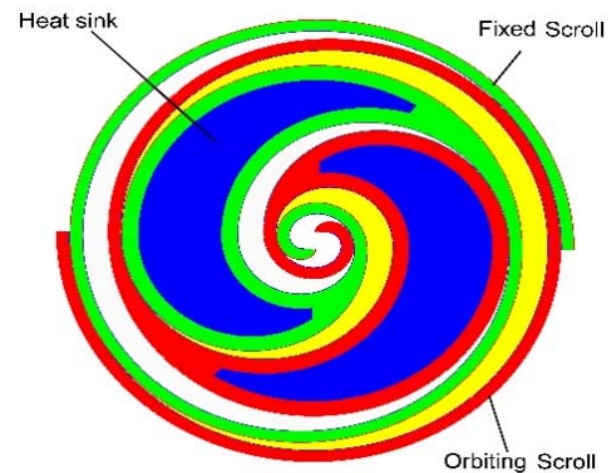
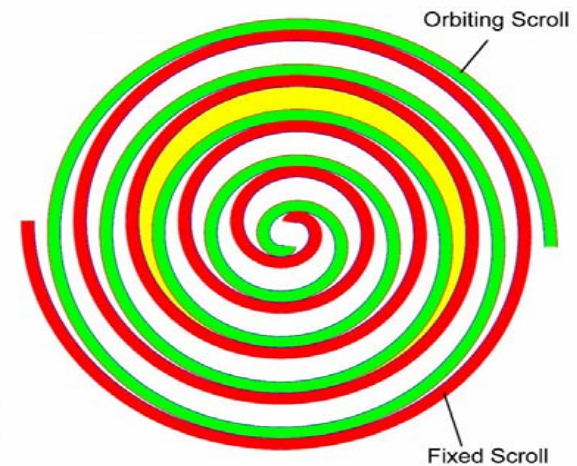


modified

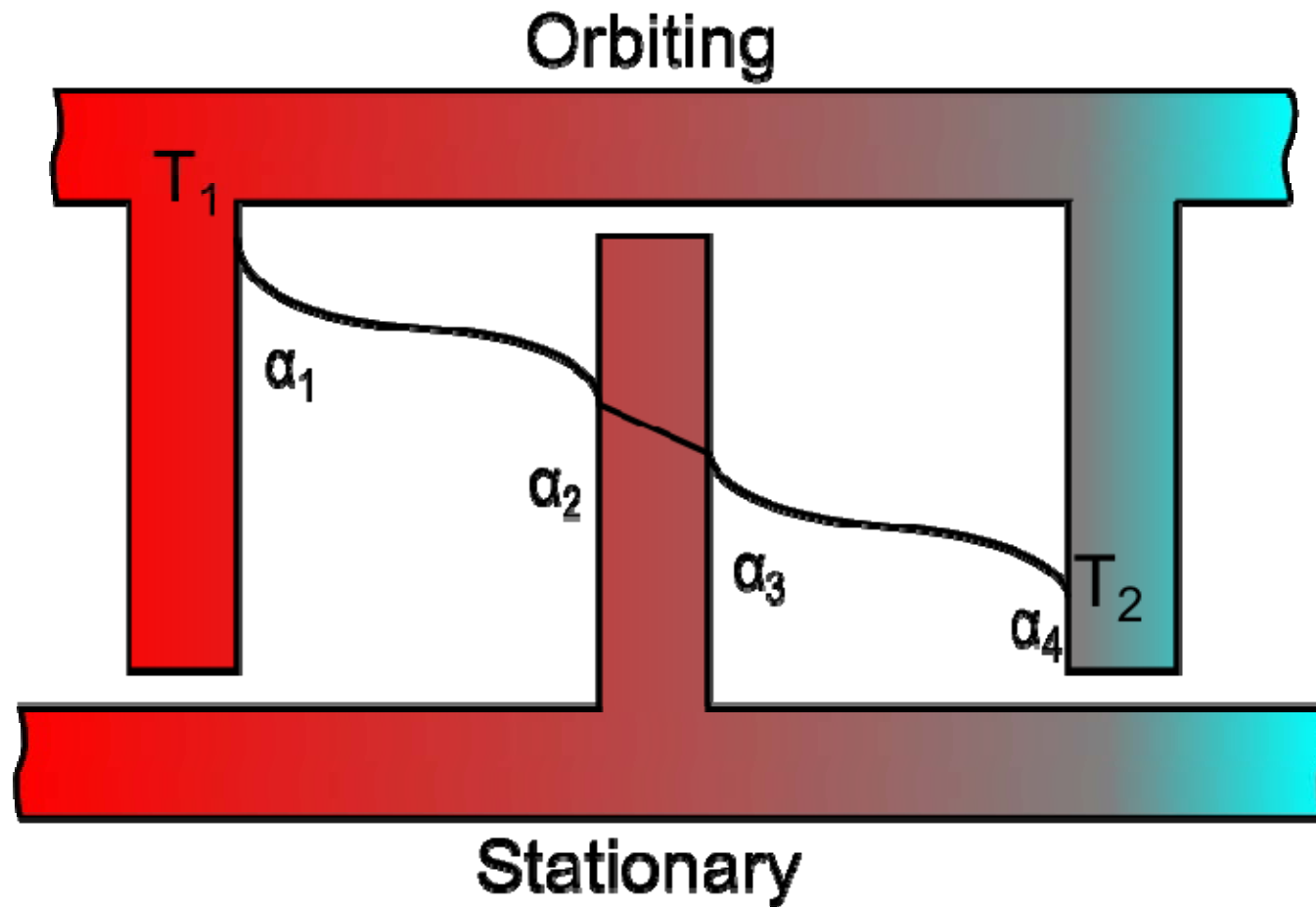


Modified vanes shape (preserved parameters)

- Vanes length reduced up to 42%
- Significant empty space inside the vanes
- Fewer working chambers – friction reduction
- Shorter compression cycle



Heat Transfer



Heat transfer coefficient [1]

$$\alpha = 0.023 \frac{\lambda}{D_h} Re^{0.8} Pr^{0.4} \left(1 + 1.77 \frac{D_h}{r_{ave}} \right)$$

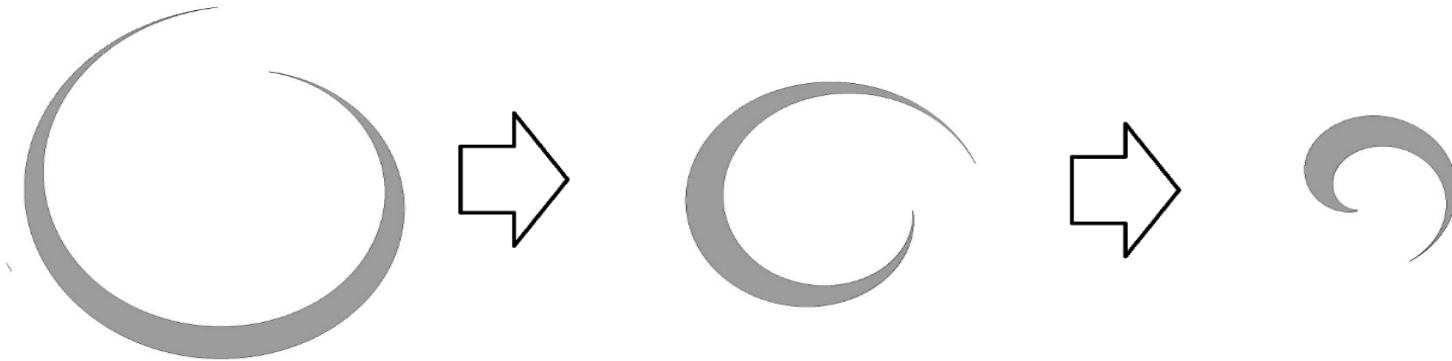
$$Re = \frac{\dot{m} D_h}{A_{cr} \mu}$$

$$D_h = \frac{4V}{A_{ar}}$$

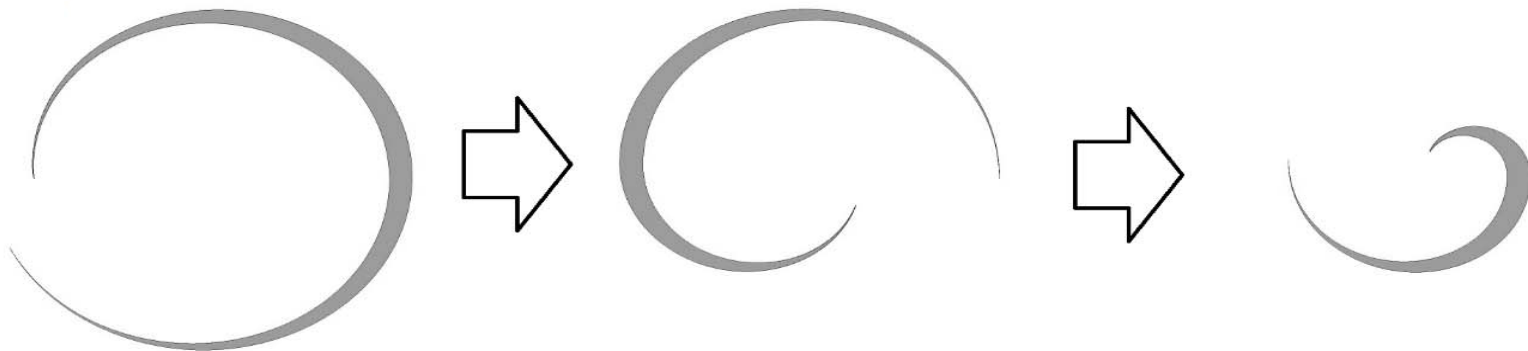
$$r_{ave} = r_b \left[\frac{(\phi_k - 0.5\pi) + (\phi_{k-1} - 0.5\pi)}{2} \right]$$



Working chambers



classic



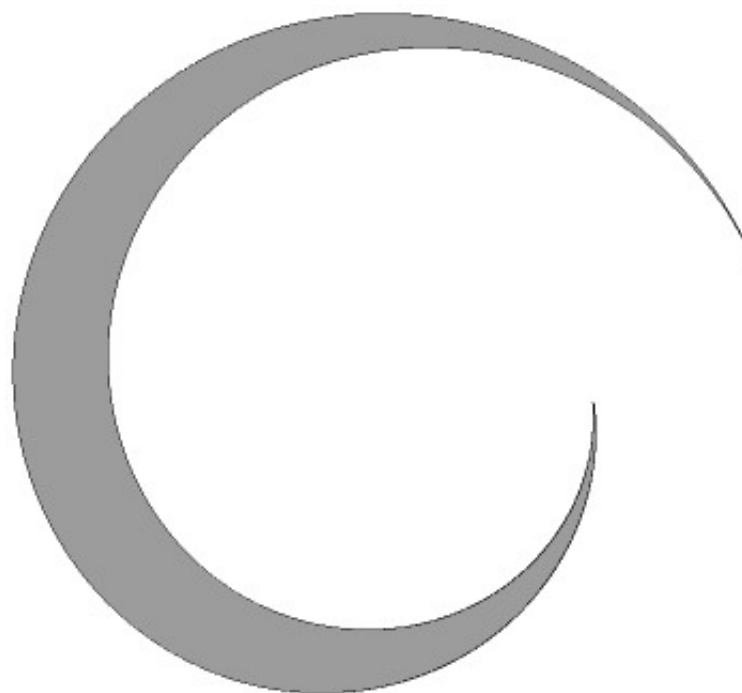
modified



Sinusoity

$$S = \frac{L}{l}$$

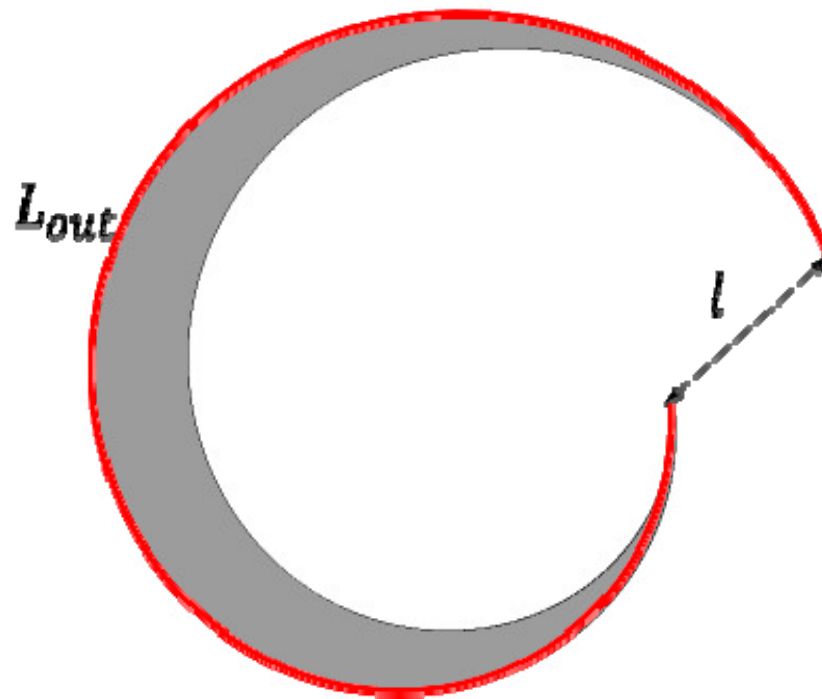
$$S = \frac{L_{out} - L_{in}}{l}$$



Sinusoity

$$S = \frac{L}{l}$$

$$S = \frac{L_{out} - L_{in}}{l}$$



CFD simulation

Medium	air, ideal gas
Suction pressure	1 bar
Suction temperature	300 K
Walls	adiabatic
Turbulence model	k-epsilon
Wall function	scalable
Scroll rotational velocity	750 and 1500 rpm
Leakage	no leakage
Vanes deformation	no deformation

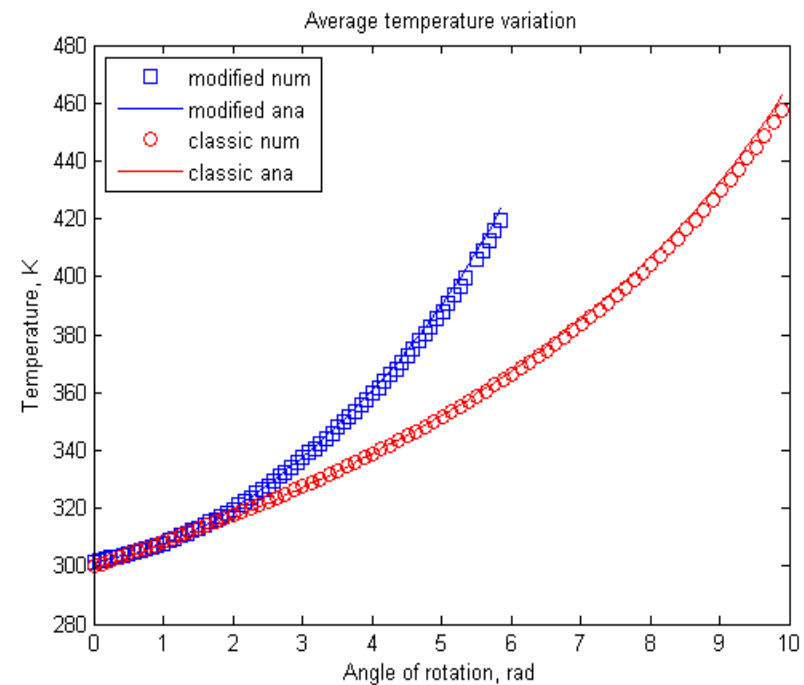
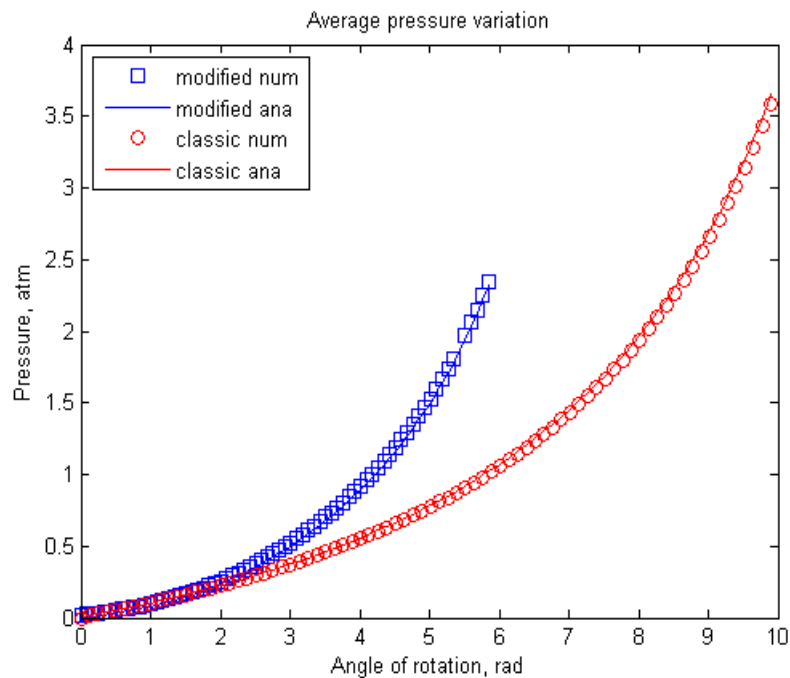


Deforming mesh

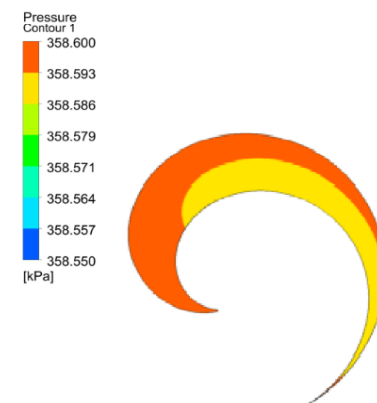
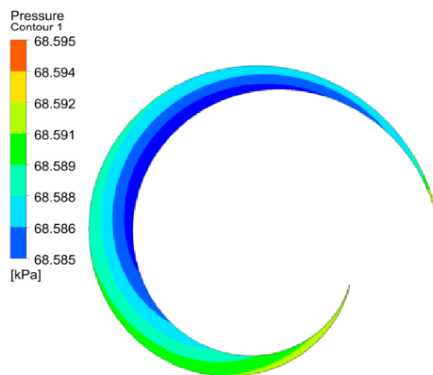
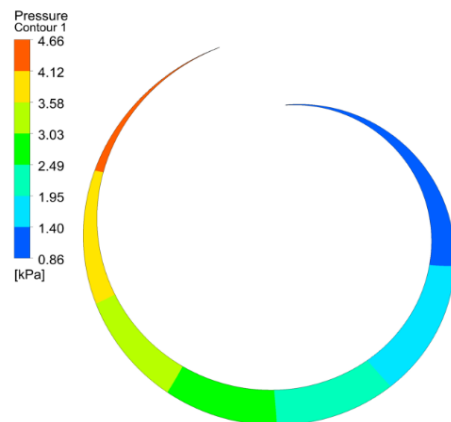
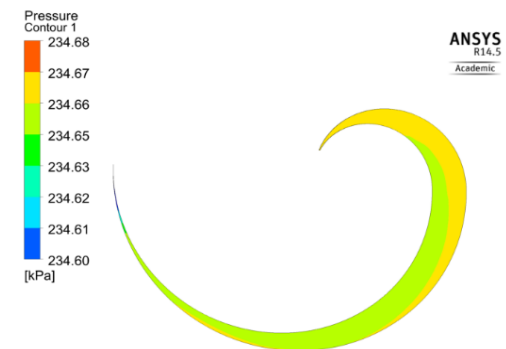
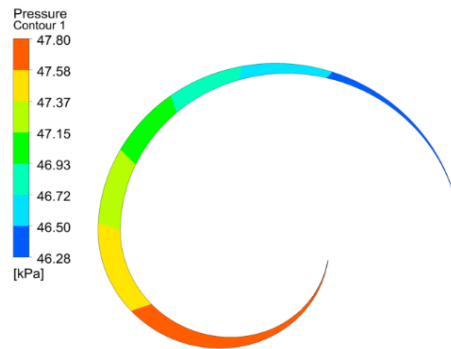
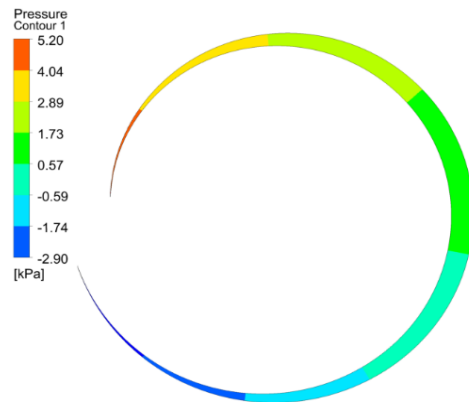
- User defined node displacement
- Ansys ICEM mesh generation script
 - automatic meshing script
 - separate mesh for each timestep
 - preserved topology
 - density as a function of timestep



Numerical vs analytical results



Pressure fields



Numerical heat transfer coefficient [2]

$$h = \frac{\rho c_p u^*}{T^+}$$

where:

$$u^* = C_\mu^{0.25} k^{0.5}$$

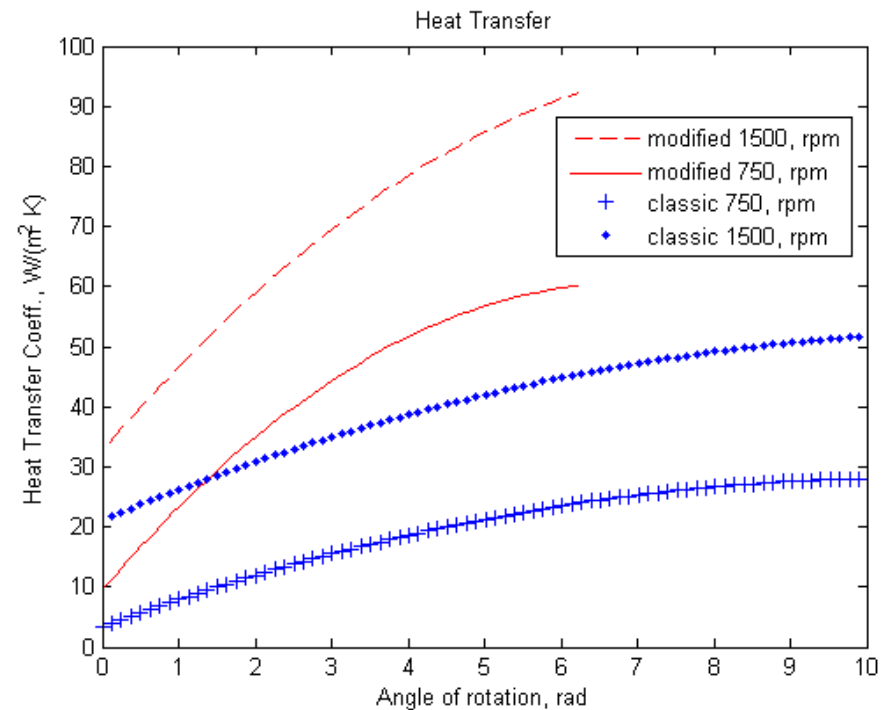
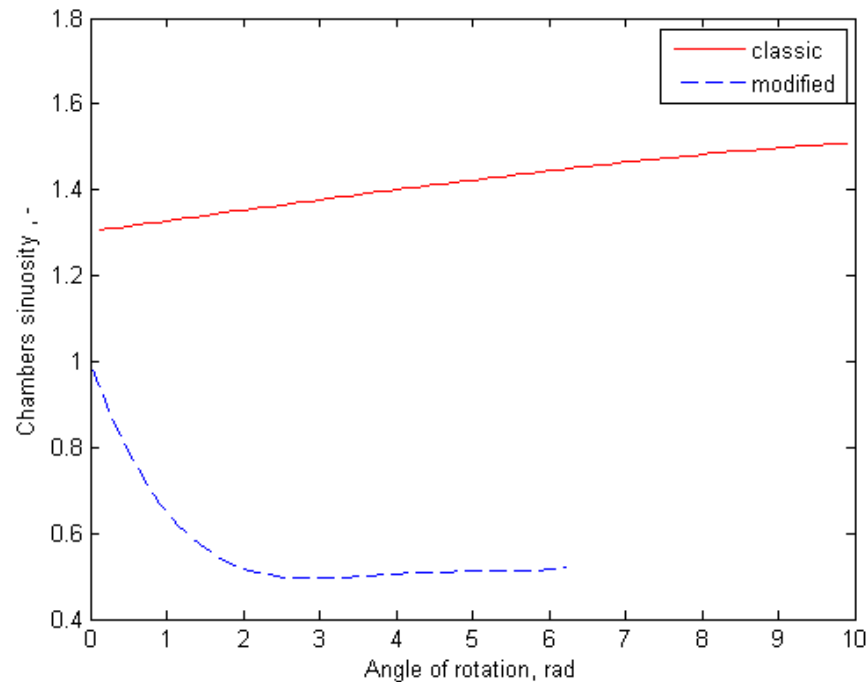
$$T^+ = 2.12 \ln y^* + \beta$$

$$\beta = \left(3.85 Pr^{\frac{1}{3}} - 1.3\right)^2 + 2.12 \ln Pr$$

$$y^* = \frac{u^* \cdot \Delta n / 4}{\nu}$$



Sinuosity and heat transfer coeff.



Summary

- New shape based scroll compressor development
- Heat transfer coefficient study
- Working chamber geometry influence on the process



References

- [1] L.C. Burmeister, Convective Heat Transfer, Wiley, New York, 1983
- [2] Ooi K.T., Zhu J., 2004, *Convective heat transfer in a scroll compressor chamber: a 2-D simulation*, International Journal of Thermal Sciences, vol. 43, no. 7, p. 677-688

