

Selection of flapper valve steel for high efficient compressor

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Outline

1. Introduction
2. Simulation on impact stress
3. Crack initiation and propagation
4. Materials investigation
5. Case studies
6. Conclusions



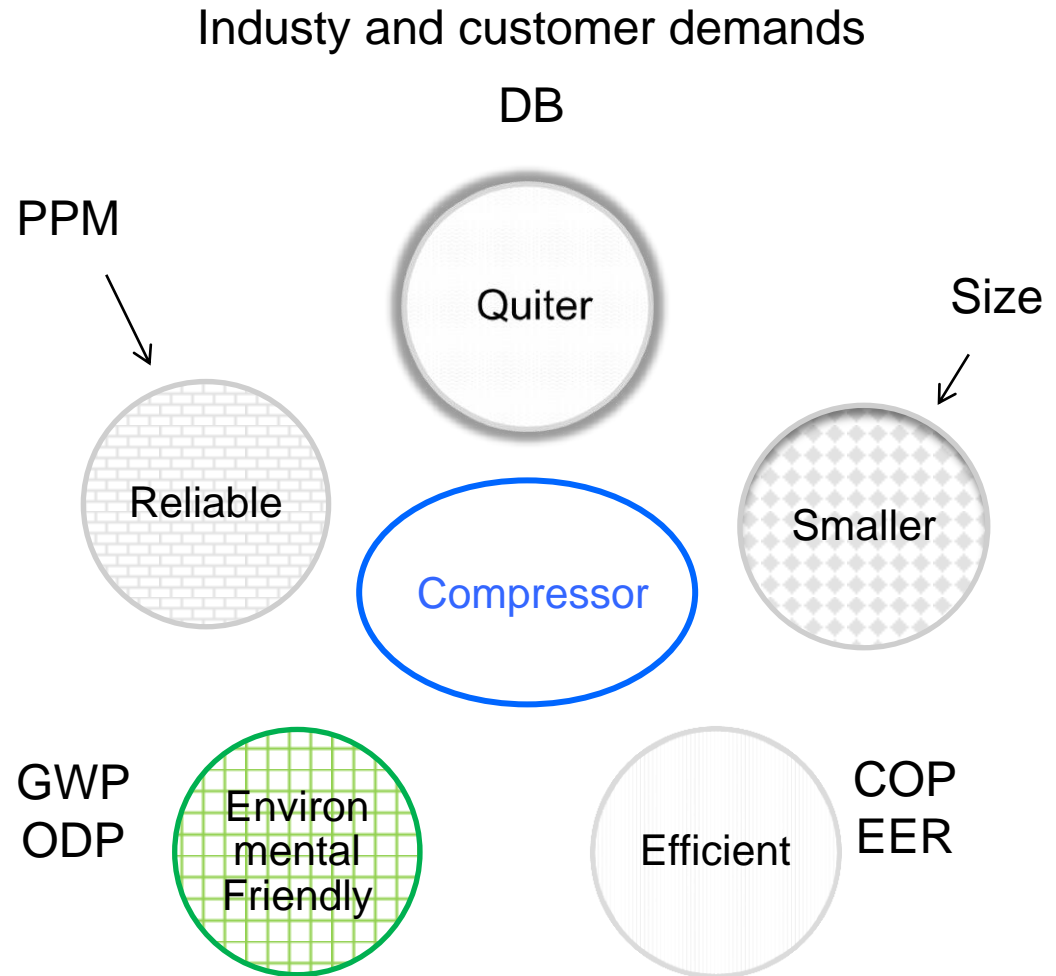
Selection of flapper valve steel for high efficient compressor



1. Introduction

Flapper valve requirements

- * Higher pressures
- * Higher temperature
- * Higher operating frequency
- * Higher discharge volume
- * Higher valve lift
- * Reduced thickness
- * Reduced valve length





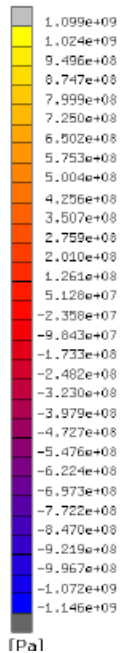
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2. Simulation of impact stress

Top

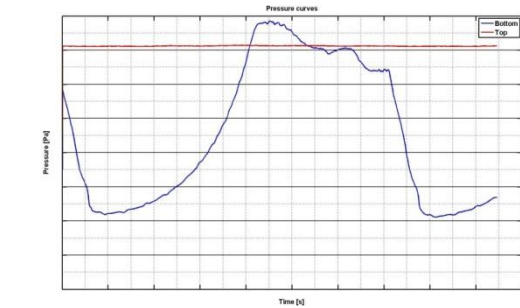
Bottom



lcase3
Major Principal Value of Stress



lcase3
Major Principal Value of Stress



FE software MSC. Marc 2011r1
 Seat of cast iron (E – modulus 130 GPa)
 Max bending stress 260 MPa
 Damping not included

Physical property	Value
Young's modulus, E [GPa]	210
Poisson's ratio, ν	0.3
Density, ρ [kg/m ³]	7700

At 7.8 m/s
 Max stress level:
 Top 1099 MPa
 Bottom -1146 MPa

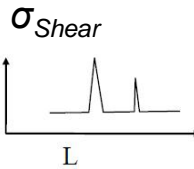
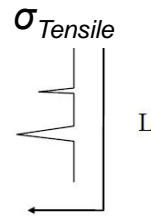
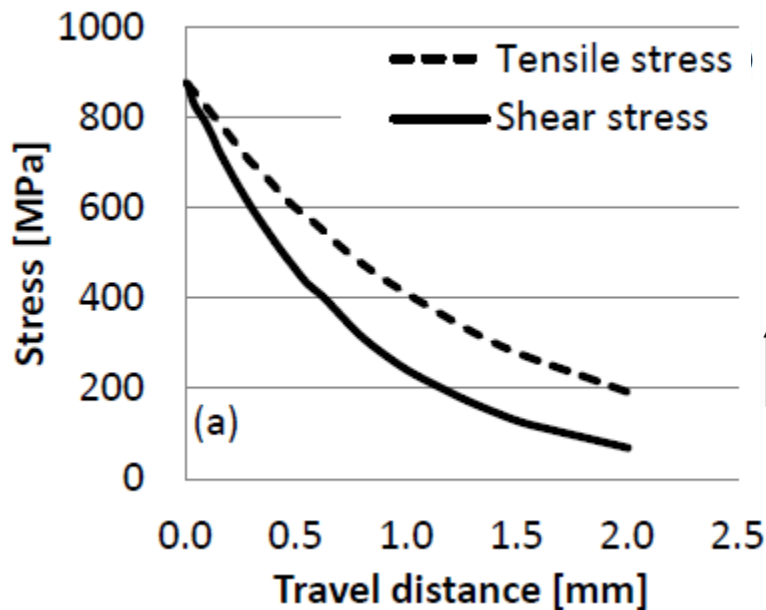




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3. Crack initiation and propagation



$$\sigma = \sigma_0 e^{-\left(\frac{tA\sqrt{E\rho}}{m}\right)} \text{ where } t = \frac{L}{C_i}$$

$$C_1 = \sqrt{E/\rho} \quad C_2 = \sqrt{G/\rho} \quad \text{where } G = \frac{E}{2(1+\nu)}$$

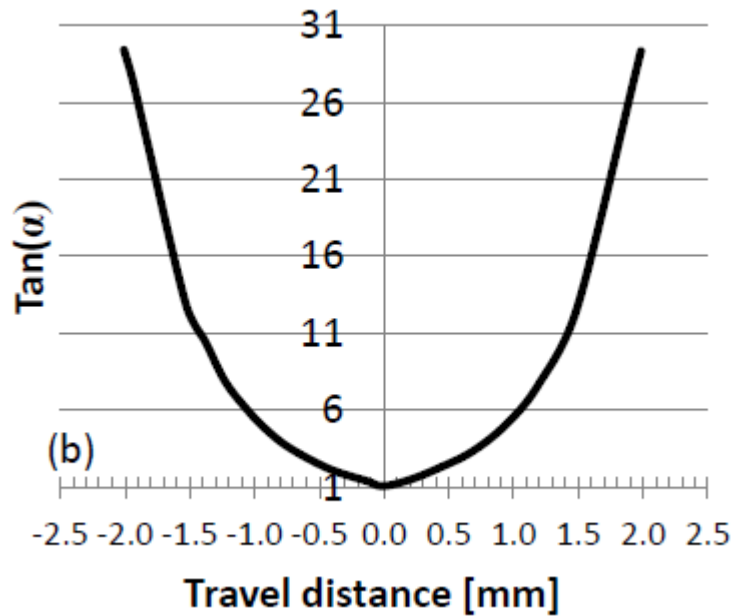
$$\sigma = \sigma_0 e^{-\frac{LA\sqrt{E\rho}}{mC_i}}$$

$$\tan(\alpha) = \frac{\sigma_{Tensile}}{\sigma_{Shear}}$$

- σ damped impact stress
- σ_0 undamped stress
- t travel time
- A Impact area
- M mass of material
- ρ density
- E Elasticity modulus
- G Shear modulus
- ν Poissons ratio
- L wave travel distance
- C_1 Tensile wave velocities
- C_2 Shear wave velocities



3. Crack initiation and propagation



$$\sigma_{Tensile} = \sigma_0 e^{-\frac{LA\rho}{m}}$$

$$\sigma_{Shear} = \sigma_0 e^{-\frac{LA\rho}{m} * 2(1+\nu)}$$

$$Tan(\alpha) = \frac{\sigma_{Tensile}}{\sigma_{Shear}}$$

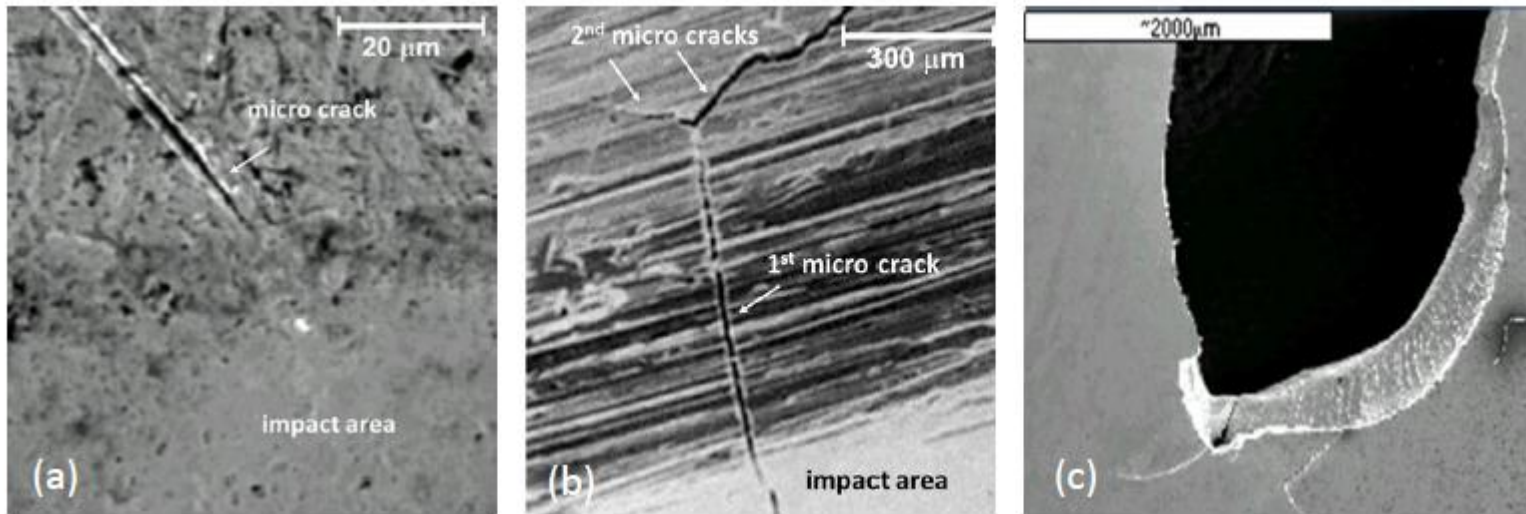


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3. Crack initiation and propagation

Fatigue crack initiation and propagation during impact



- a) Crack initiation
- b) Splitting of main crack
- c) Formation of chipping

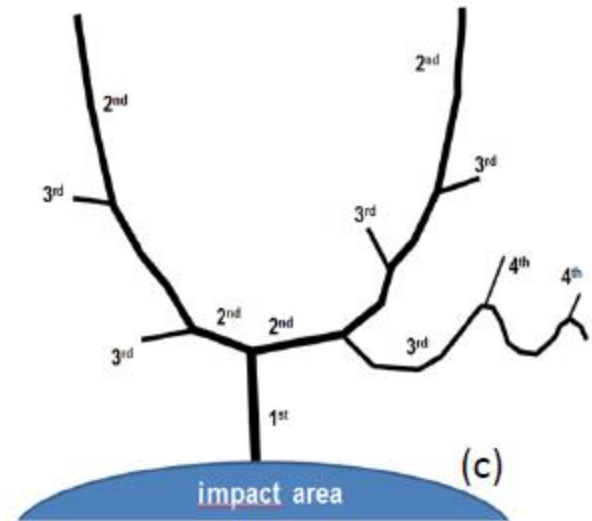
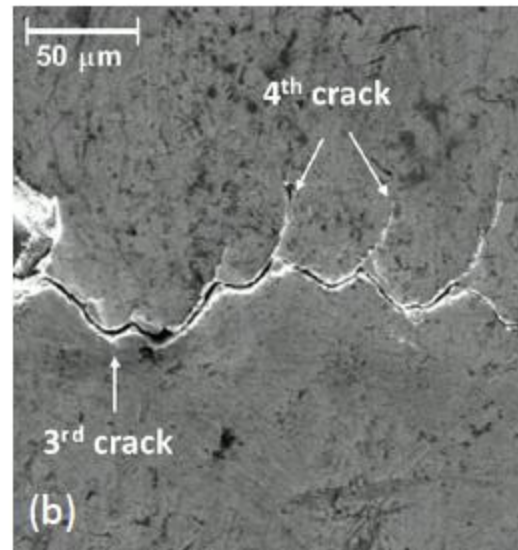
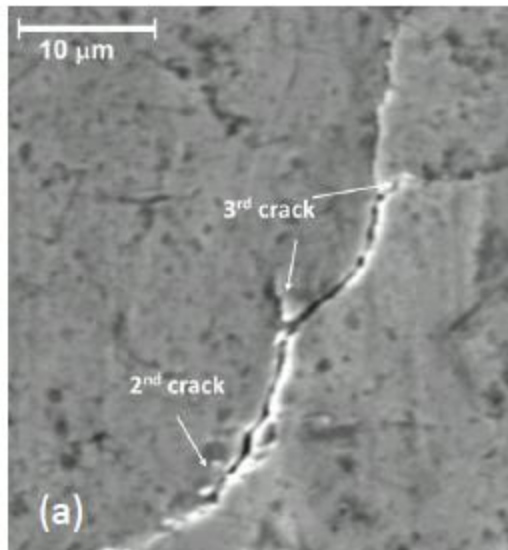


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3. Crack initiation and propagation

Fatigue crack initiation and propagation during impact



- a) Along radial direction
- b) Along transversal direction
- c) A fracture model based on dynamic stress wave theory



3. Crack initiation and propagation

This analysis indicates that a material with high impact fatigue strength should have:

- 1). High resistance to crack initiations and propagations by repeated impact loading
- 2). High stress decay rate to stress wave travelling so that the crack propagation becomes difficult.



4. Materials investigation

Investigation of 3 different flapper valve steels materials

Sandvik 20 C

AISI 1095

Sandvik 7C27Mo2

mod AISI 420

and

Sandvik Hiflex™

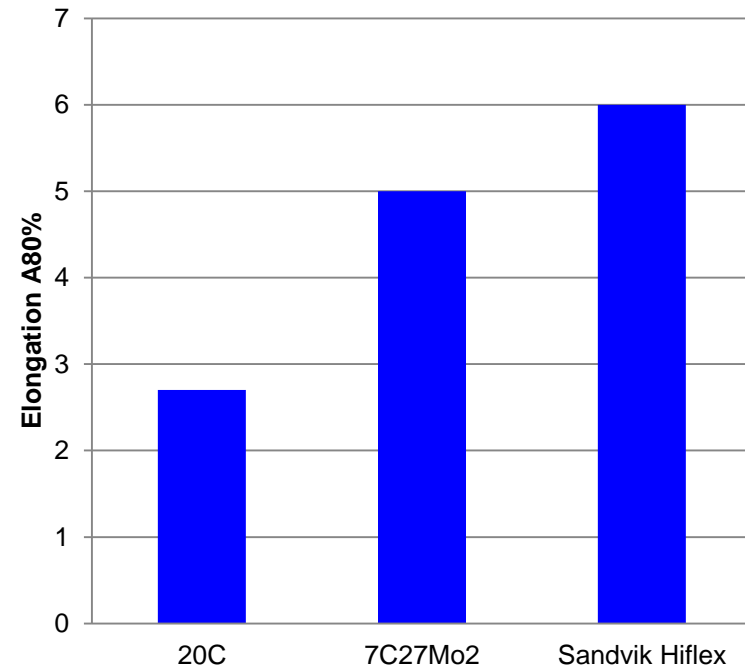
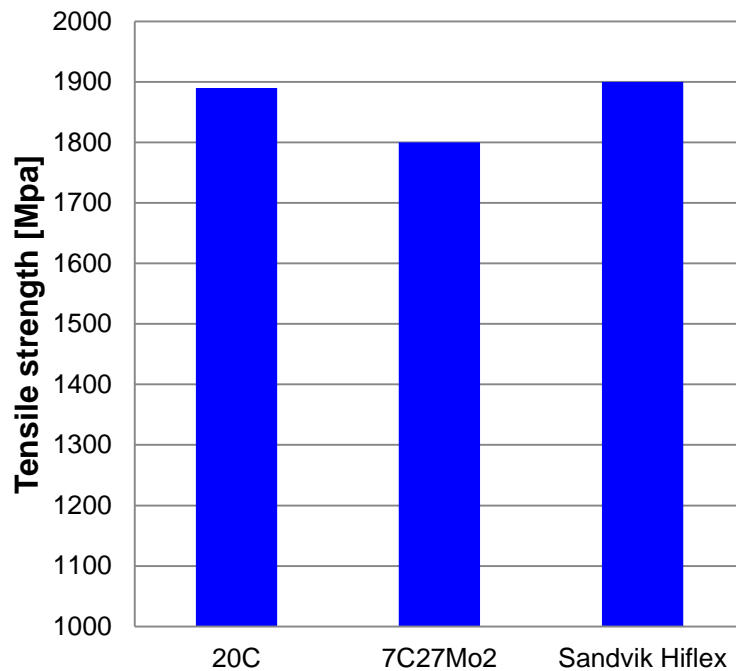
(which is a type of modified AISI 420 material)



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4. Materials investigation



Hiflex has a higher tensile strength but also elongation than the other investigated materials

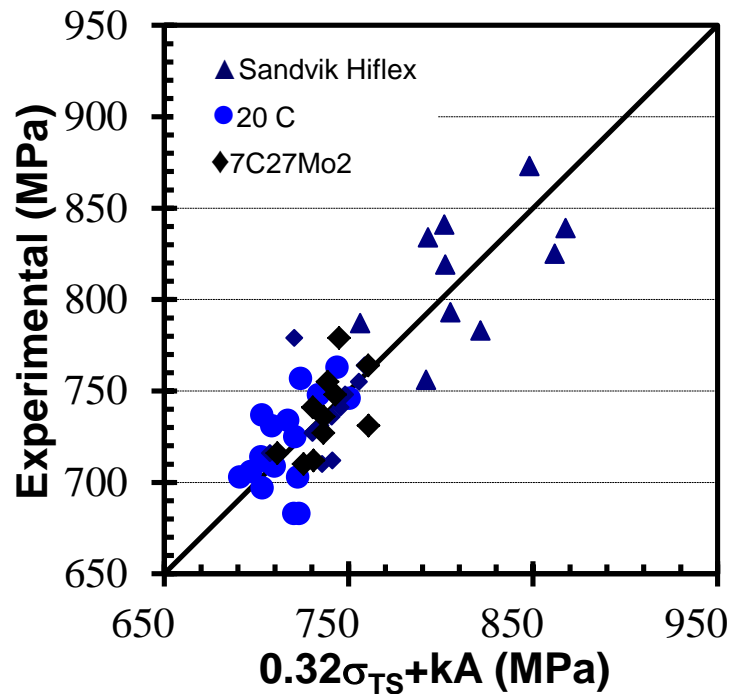


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4. Materials investigation

Bending fatigue vs tensile strength σ_{TS} and ductility/elongation A



K is a constant between 18.8 and 25.1 depending on material.

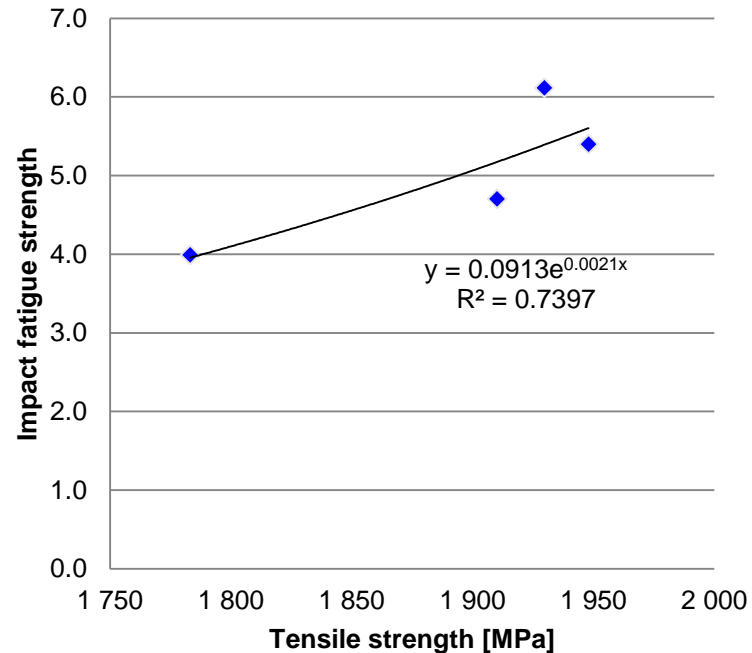


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4. Materials investigation

Impact fatigue vs tensile strength



A weak correlation between impact fatigue and tensile strength.

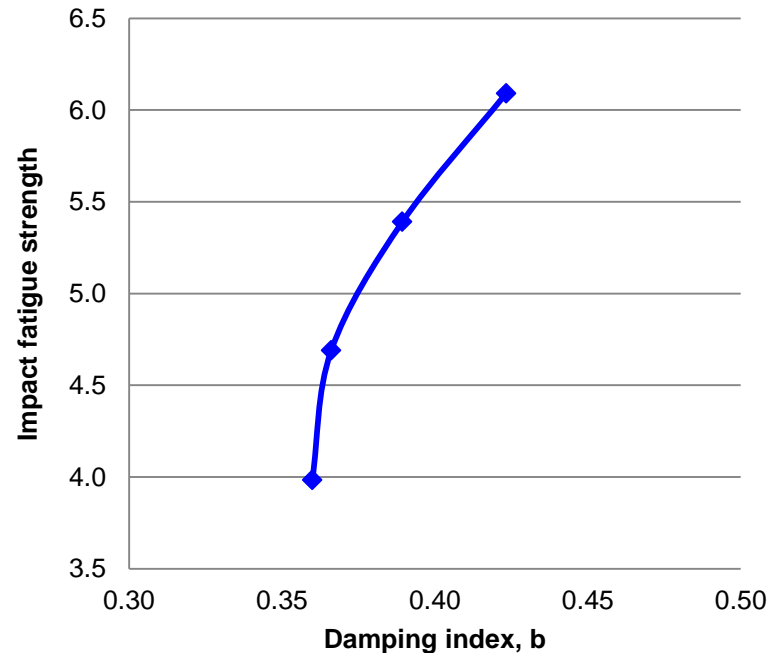


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4. Materials investigation

Material with similar
E – modulus
Density
But
different damping capacity



$$A = A_0 e^{-bt}$$

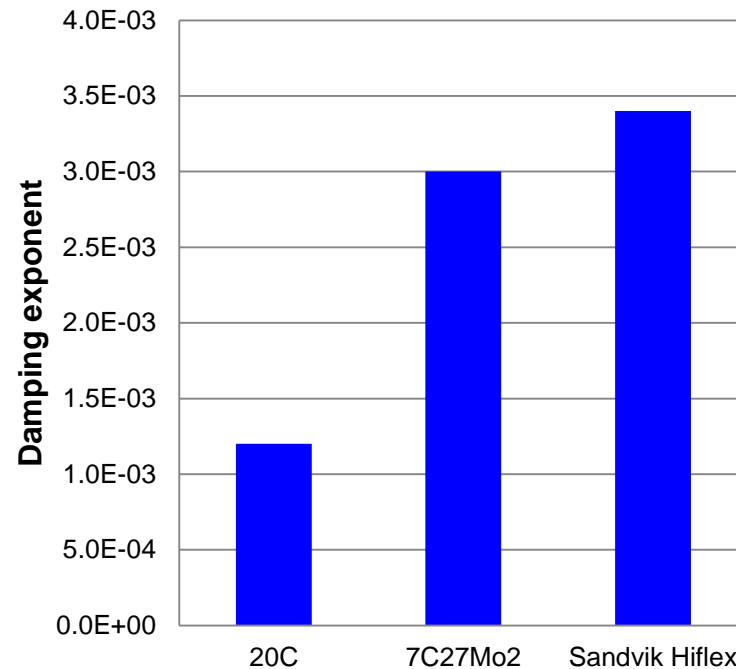
A higher damping index may result in a higher impact fatigue limit



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4. Materials investigation



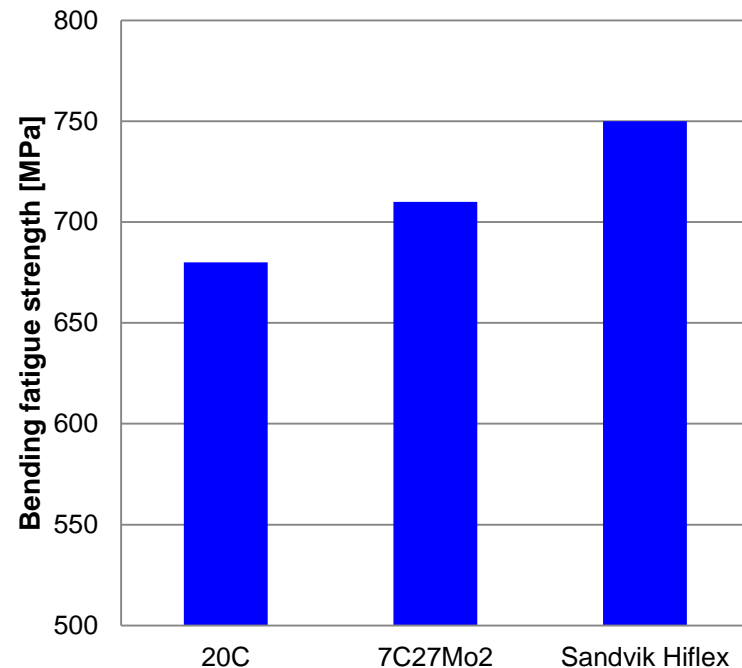
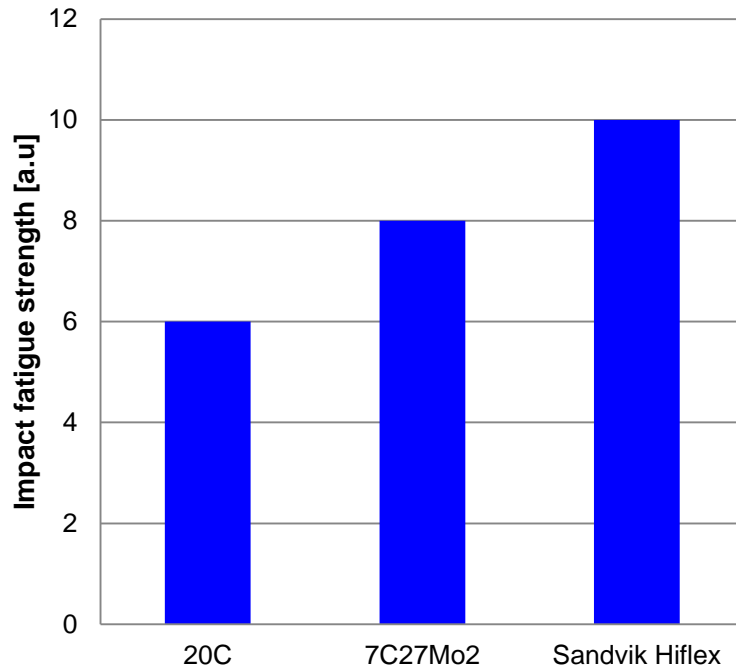
The damping exponent for the different flapper valve steels



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4. Materials investigation



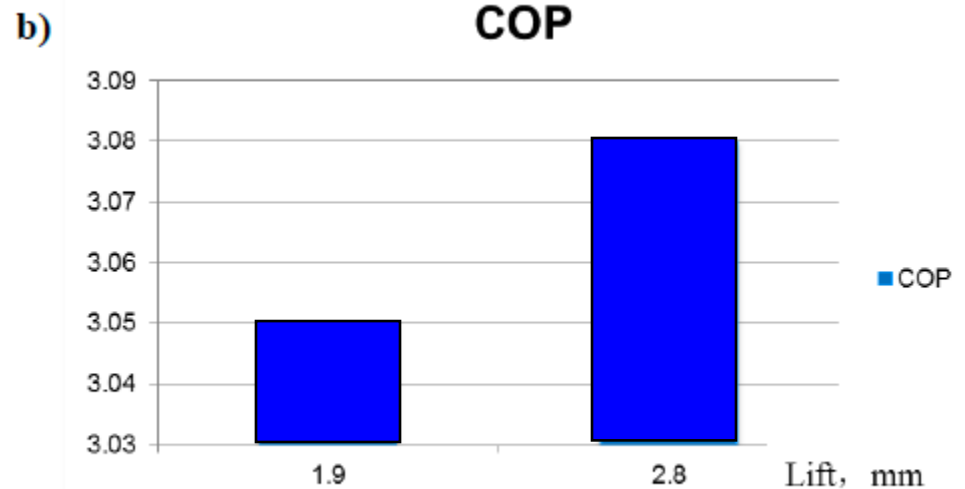
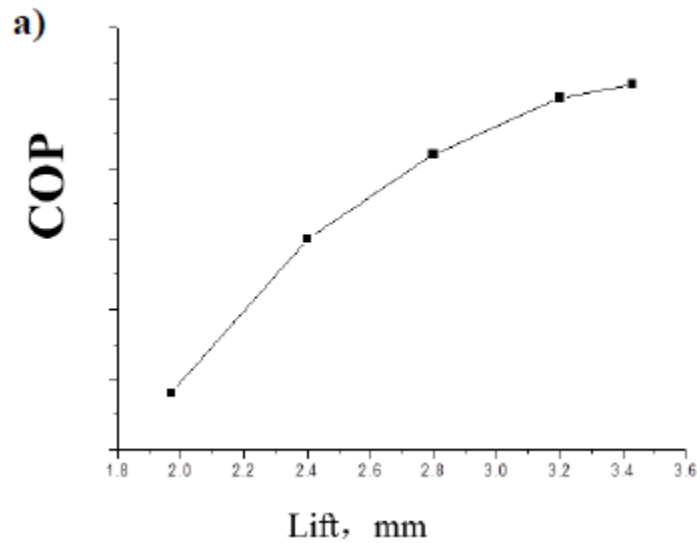
Hiflex exhibit a higher impact fatigue strength and bending fatigue strength than the other investigated materials



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5. Case studies



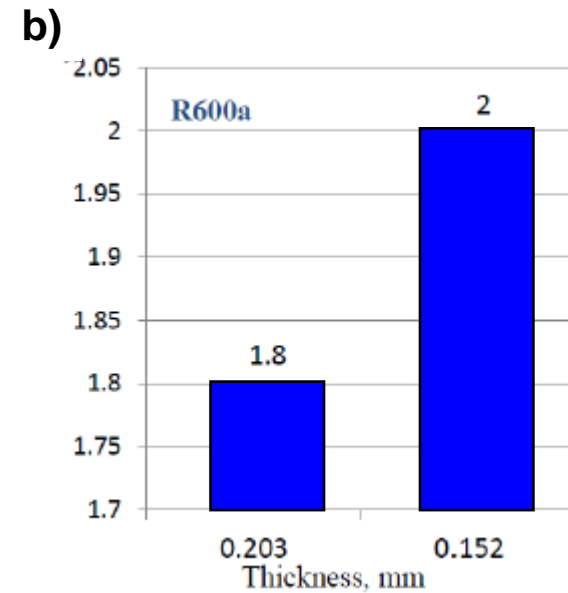
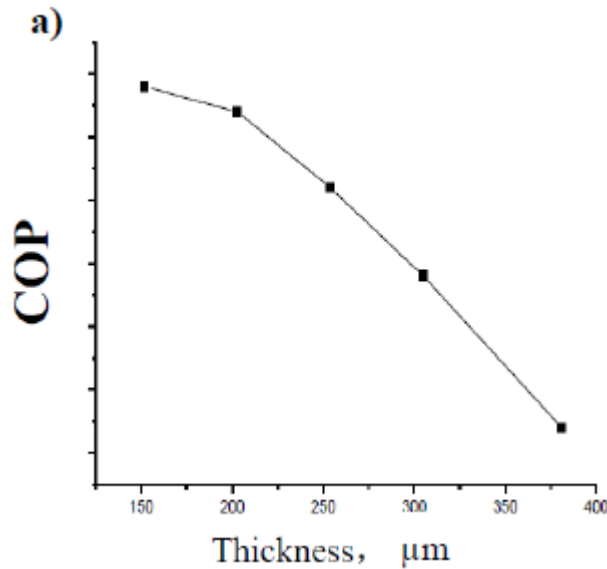
- a) COP as a function of valve lift
- b) Specifically values on COP for 1.9 and 2.8 mm valve lift in a refrigerant of R22 at a compressor manufacturer



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5. Case studies



a) COP as a function of valve thickness

Specifically values on (at compressor manufacturer)

b) COP for 0.203 mm and 0.152 mm in a refrigerant of R600a



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5. Case studies



Examples of



- a) A failed 7C27Mo2 valve
- b) A well – functioning valve of Sandvik Hiflex together with seat



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5. Case studies

Refrigerant: R410a		
P_d P_s	3.40 MPa 0.55 MPa	3.40 MPa 0.55 MPa
Operating frequency	120 Hz	180 Hz
Discharge volume	80 cc	80 cc

An example of usage of 7C27Mo2 to tough conditions. When replaced with Sandvik Hiflex the valve managed the test.



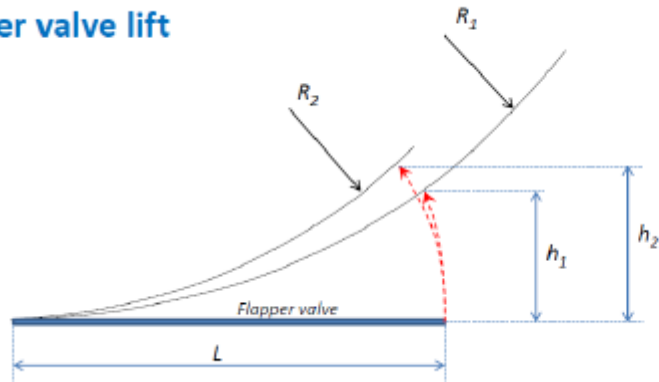
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5. Case studies

Higher valve lift

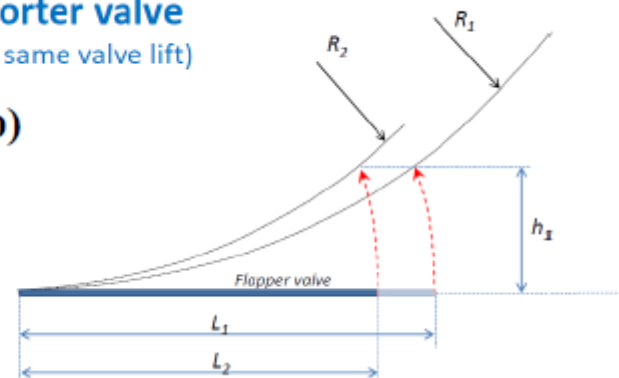
(a)



Shorter valve

(the same valve lift)

(b)



The higher impact and bending fatigue limits of Sandvik Hiflex lead to improved design freedom due to the following

- * Higher valve lift
- * Reduced thickness
- Reduced valve length
- Higher damping



Selection of flapper valve steel for high efficient compressor



6. Conclusions

The stresses that cause the fatigue damage or fracture are the tensile stress wave and shear stress wave induced by repeated impact loading.

- Due to combined stress waves, initiated micro-cracks propagate in waveforms in the transversal direction, and new cracks will initiate at the stress concentration peaks of the original crack. The propagation of new cracks in radial directions leads to edge chipping.
- The crack formation and propagation analysis indicate that a flapper valve material with high performance or fatigue strength should have;
 - high resistance to crack initiations and propagations, by high tensile strength and high ductility
 - high stress decay rate with stress wave travelling so that the crack propagation becomes difficult.
- Sandvik Hiflex™ shows high tensile strength, high bending and impact fatigue strength and high damping capacity, which shows excellent performance in the newly developed high efficient compressors.



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Thank you
for
your
attention