
Generalized heuristic control for direct expansion (DX) cooling systems with capacity modulation and variable air flow

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Outline



- Introduction
- Component models
- Fan-duct systems
- Optimal operations
- Control heuristics
- Energy saving assessment with simulation



Introduction



Motivation:

- Direct expansion (DX) air conditioning systems are widely used in small- to medium-sized commercial buildings
- More DX units are equipped with variable speed drives (VSD) since VSD becomes more affordable
- Need an implementable and model-free control strategy

Approach:

- DX units with different types of compressors are modeled from catalog data
- Different fan-duct system characteristics are considered
- Optimization is performed to the integrated system model
- Obtain a generalized control heuristics from the optimal results



DX models



Component-model descriptions:

Compressor

- Empirical catalog model

Condenser & evaporator

- Effectiveness-NTU method
- Correlate heat transfer coefficients to air and refrigerant mass flow rates

Input-output forms :

$$\left[P_{comp}, m_r \right] = Compressor \left(\underline{T_{evap}}, \underline{T_{cond}}, \underline{Stage} \right)$$

$$\left[q_{tot}, q_{sen} \right] = Evap \left(\underline{T_{evap}}, \underline{V}, \underline{T_{air,db,evap}}, \underline{T_{air,wb,evap}} \right)$$

$$q_{cond} = Cond \left(\underline{T_{cond}}, \underline{T_{amb}}, m_r \right)$$

X : external inputs (boundary condition).

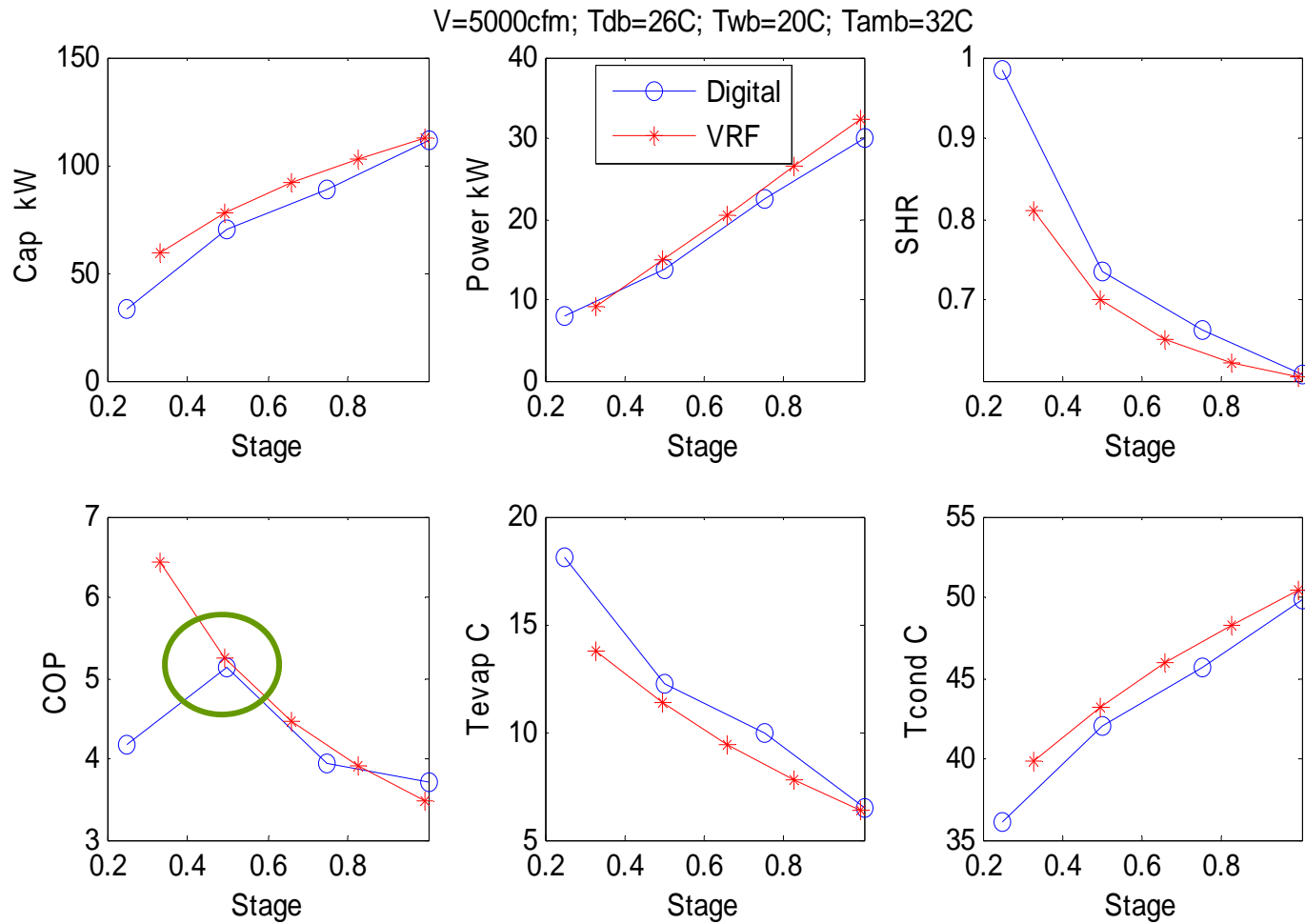
X : internal variables that need to be solved iteratively

Model integration: Solve $\begin{cases} q_{tot} + 0.95 \times P_{comp} = q_{cond} \\ T_{sc} = 15 \text{ F} \end{cases}$ for $\begin{bmatrix} T_{evap} \\ T_{cond} \end{bmatrix}$

Input-output form: $\left[P_{comp}, q_{tot}, SHR, T_{sup} \right] = DX \left(T_{air,db,evap}, T_{air,wb,evap}, T_{amb}, V, Stage \right)$

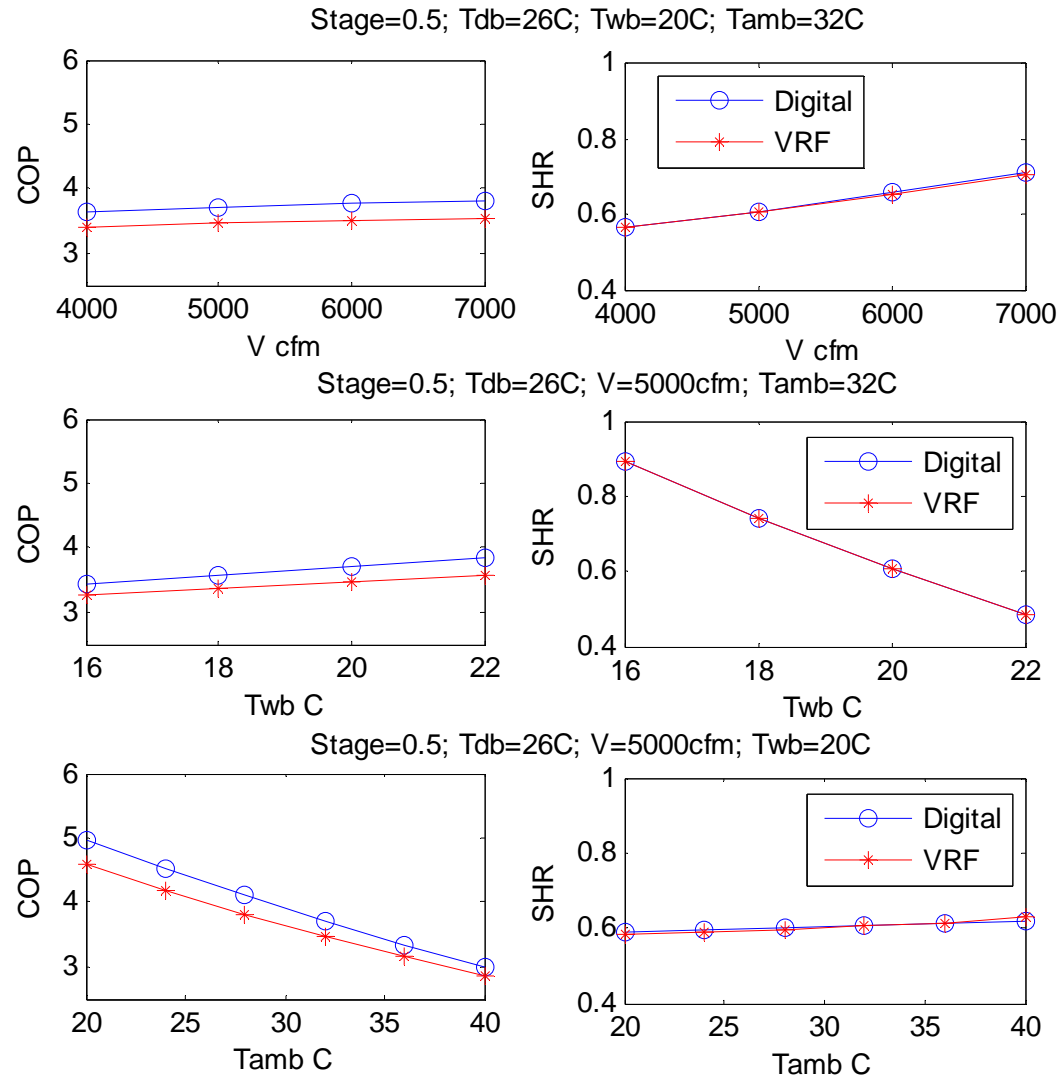


Integrated model





Integrated model





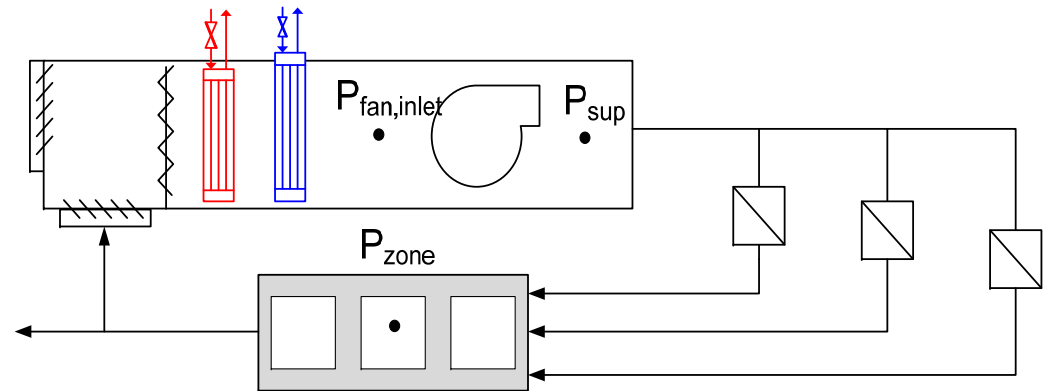
Duct system characteristics



$$ESP = \Delta P_{fan,downstream} + \Delta P_{fan,upstream}$$

$$\Delta P_{fan,downstream} = P_{sup} - P_{zone} = A \cdot V^2$$

$$\Delta P_{fan,upstream} = P_{zone} - P_{fan,inlet} = B \cdot V^2$$



Constant static pressure

$$ESP = \Delta P_{fan,downstream} + \Delta P_{fan,upstream} = D + B \cdot V^2$$

Resetting static pressure

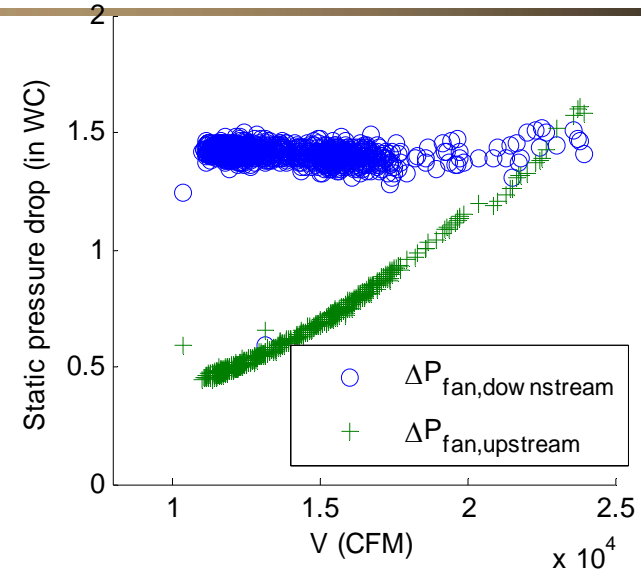
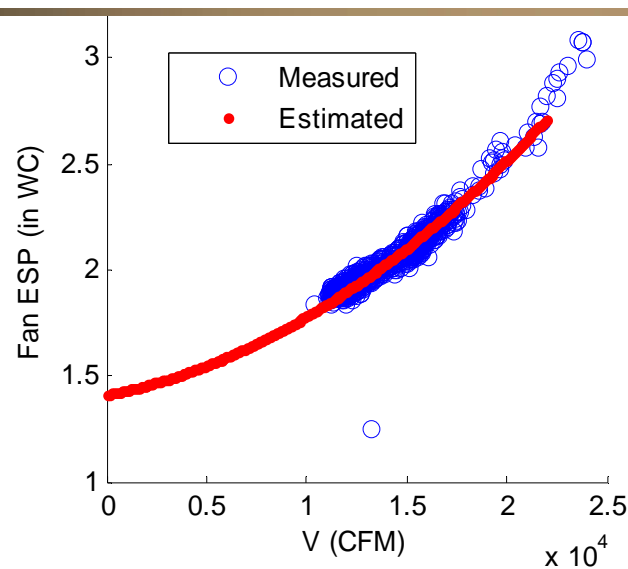
$$ESP = \Delta P_{fan,downstream} + \Delta P_{fan,upstream} = (A + B)V^2 = C \cdot V^2$$



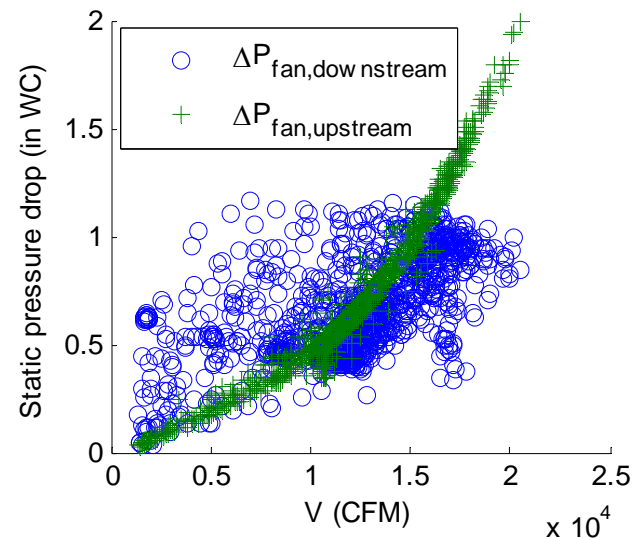
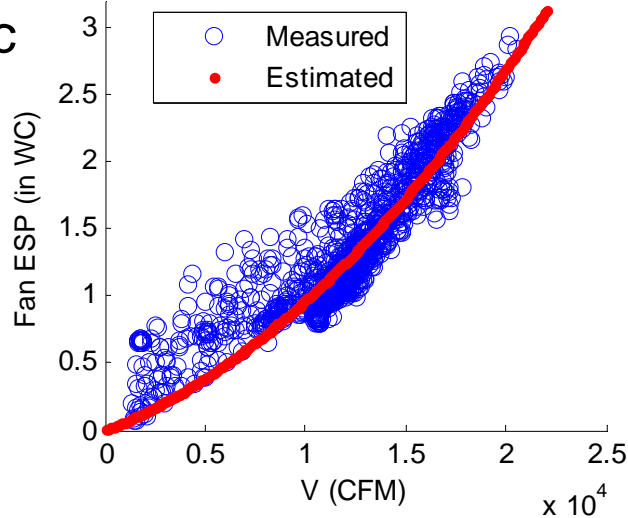
Fan-duct systems



Constant static pressure



Resetting static pressure



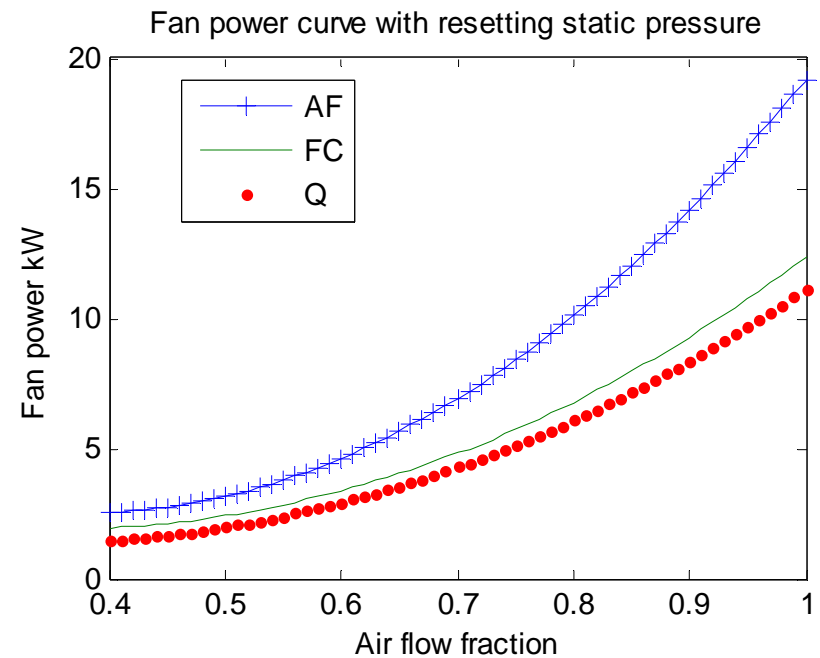
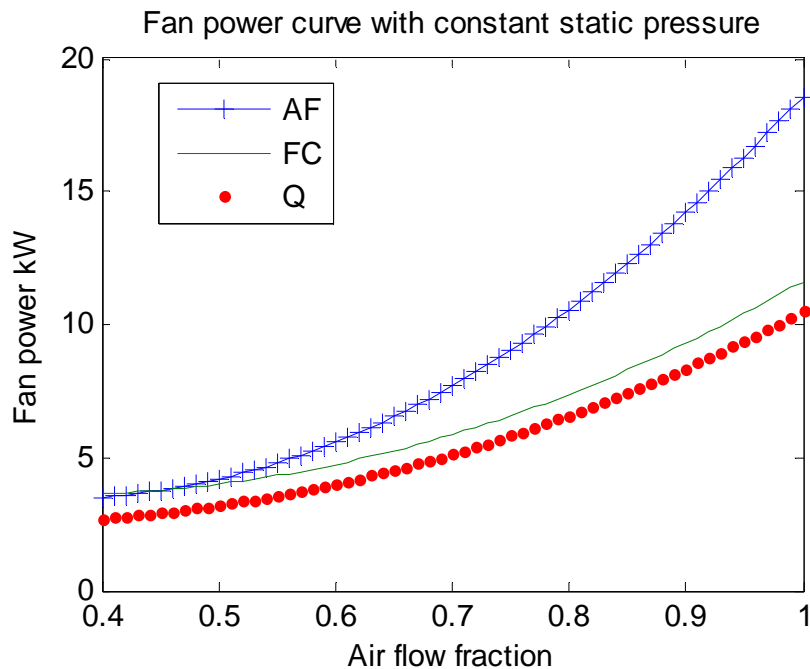


Fans



Three types of fans are considered:

	Diameter (in)	Maximum SP (inwc)	Maximum HP (bhp)
FC (forward curved)	25	5	30
AF (airfoil)	22	8	40
Q (vaneaxial)	36.5	5	30





Optimization problem formulation



Problem formulation:

$$T_{sup,opti} = \arg \min_{T_{sup}} P_{DX} \left(\overline{T_{air,db,evap}}, \overline{T_{air,wb,evap}}, \overline{T_{amb}}, V, T_{sup} \right) + P_{fan}(V)$$

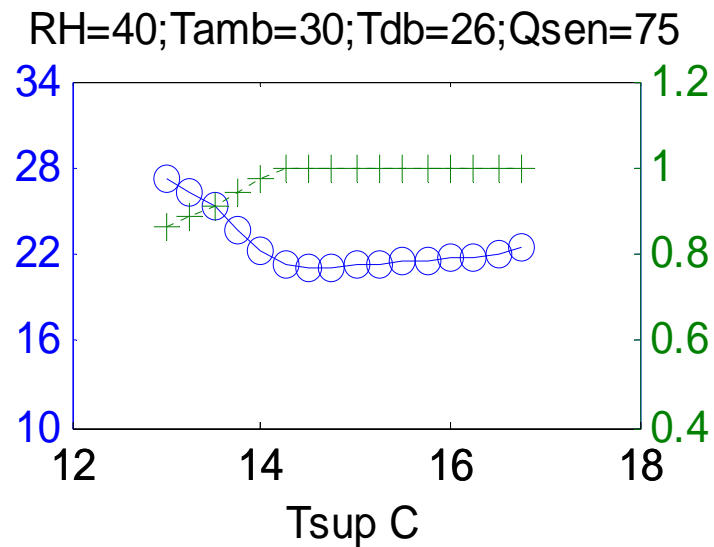
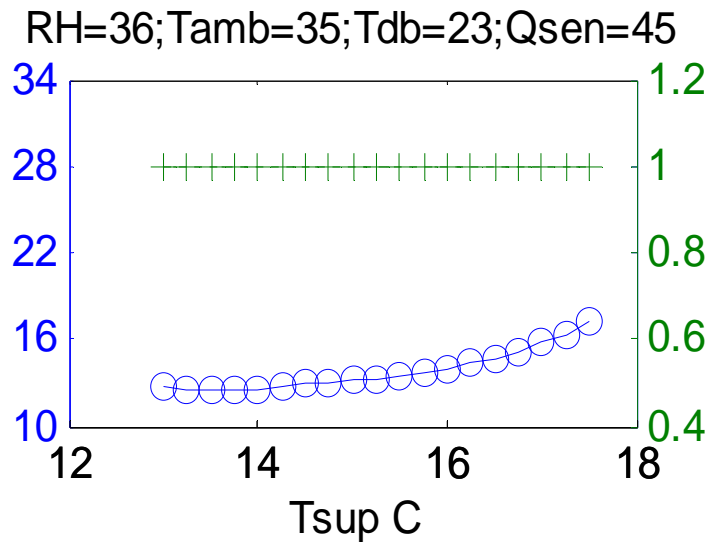
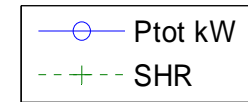
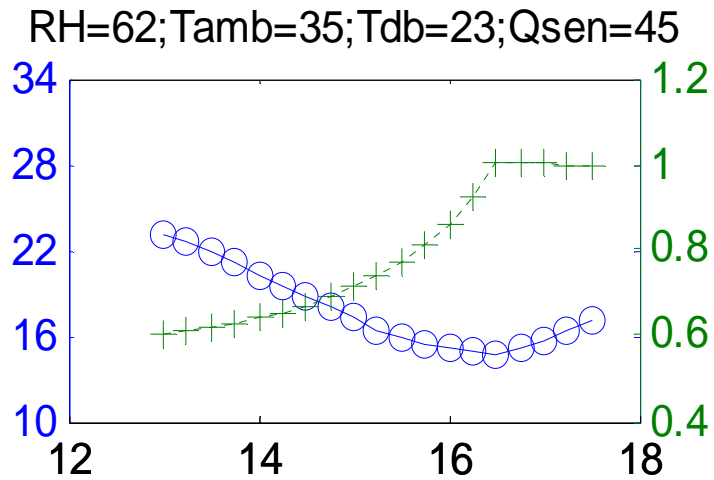
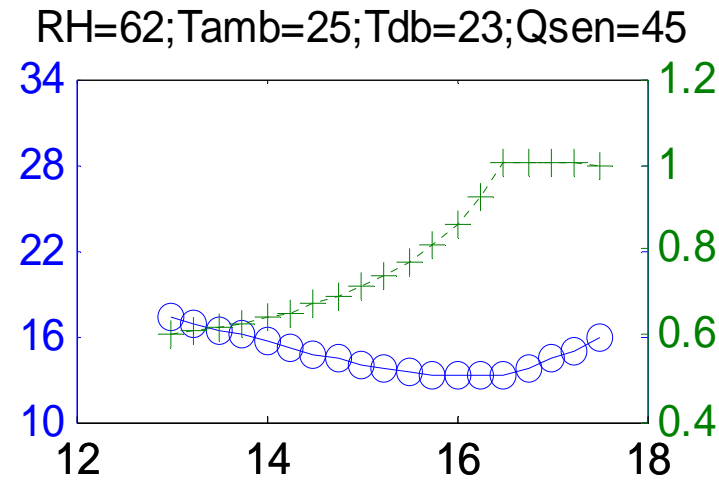
satisfying

$$\left\{ \begin{array}{l} q_{sen} = \overline{q_{sen,req}} \\ SHR < \overline{SHR}_{max} \\ V_{min} < \dot{V} < V_{max} \\ Stage \in [0,1] \\ T_{min} < T_{sup} < T_{max} \end{array} \right.$$

- SHR_{max} -- dehumidification lower limit
- Overbar variable -- boundary condition or requirements



Visualization of optimization results



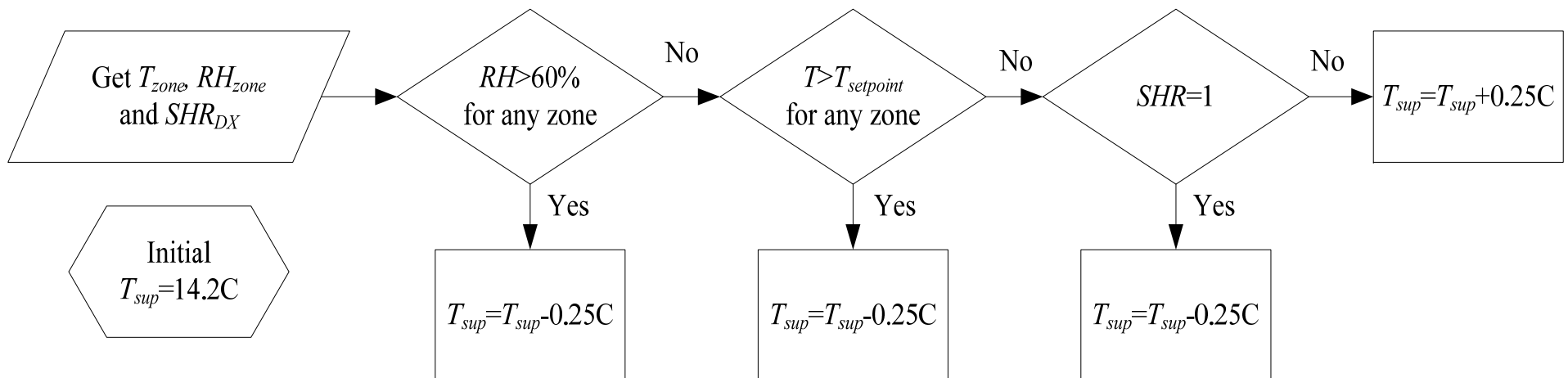


Control heuristics



Control heuristics:

Increase the supply air temperature setpoint until the SHR upper bound is reached

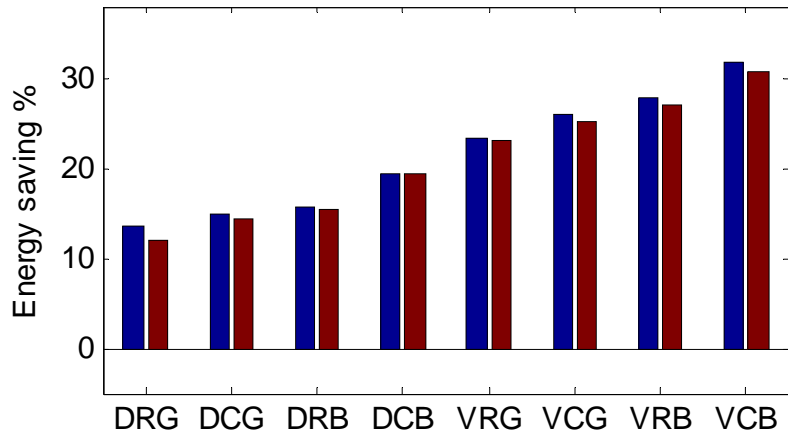




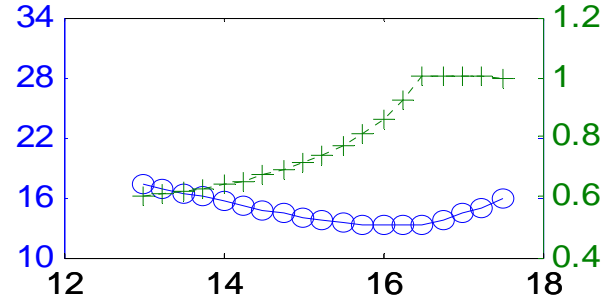
Compare heuristic & optimal control



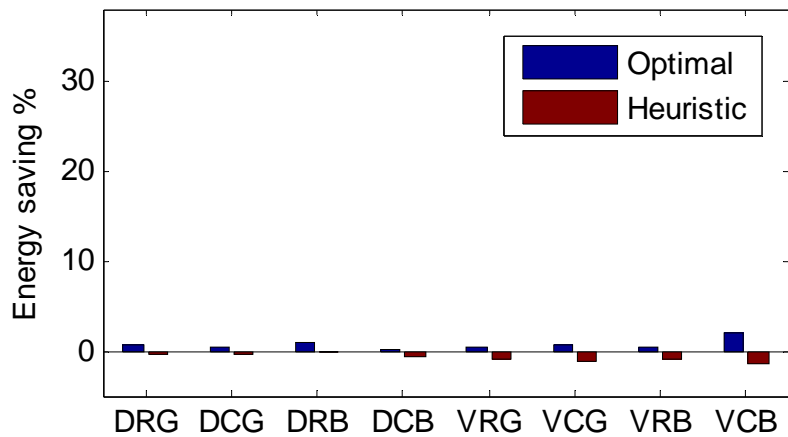
Tdb=23C; RH=62; Tamb=25C; Qsen=75kW



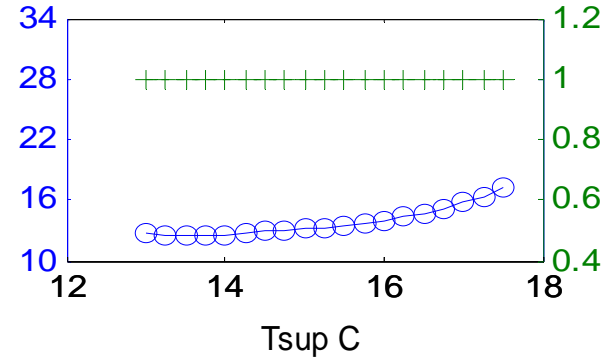
RH=62; Tamb=25; Tdb=23; Qsen=45



Tdb=23C; RH=36; Tamb=35C; Qsen=75kW



RH=36; Tamb=35; Tdb=23; Qsen=45



X labels:

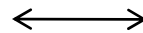
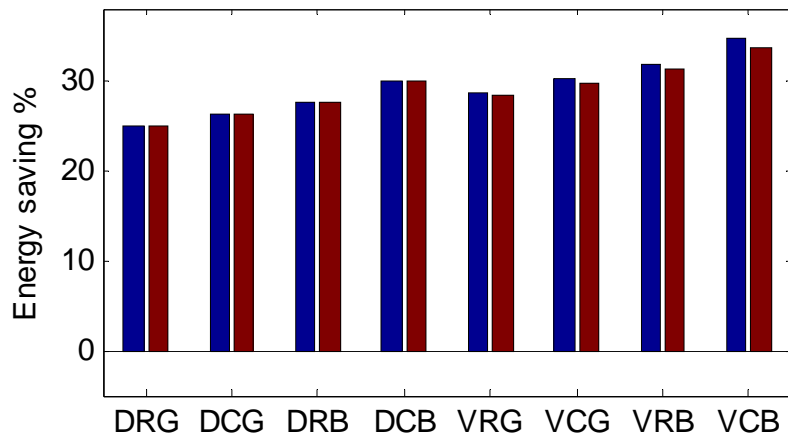
- 1st character indicates compressor type:
D-digital scroll; V-variable speed
- 2nd character indicates pressure control:
R-resetting; C-constant
- 3rd character indicates fan model series



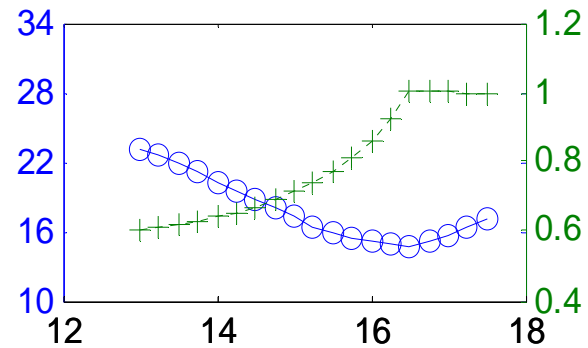
Compare heuristic & optimal control



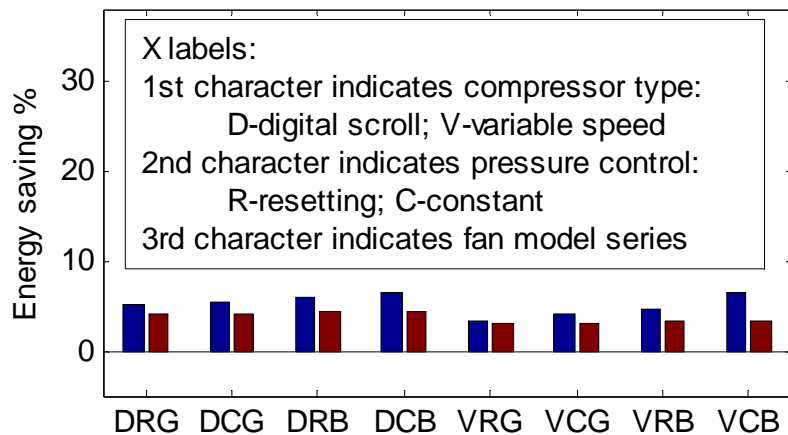
$T_{db}=23C$; $RH=62$; $T_{amb}=35C$; $Q_{sen}=75kW$



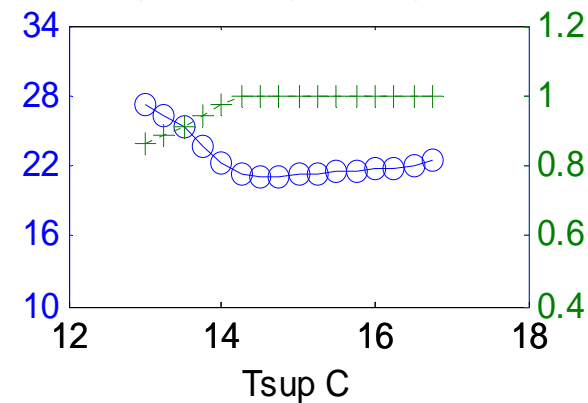
$RH=62$; $T_{amb}=35$; $T_{db}=23$; $Q_{sen}=45$



$T_{db}=26C$; $RH=40$; $T_{amb}=30C$; $Q_{sen}=75kW$



$RH=40$; $T_{amb}=30$; $T_{db}=26$; $Q_{sen}=75$



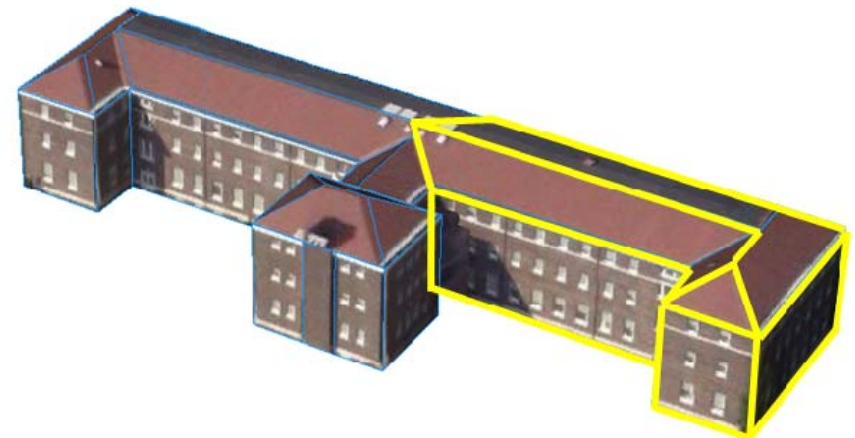
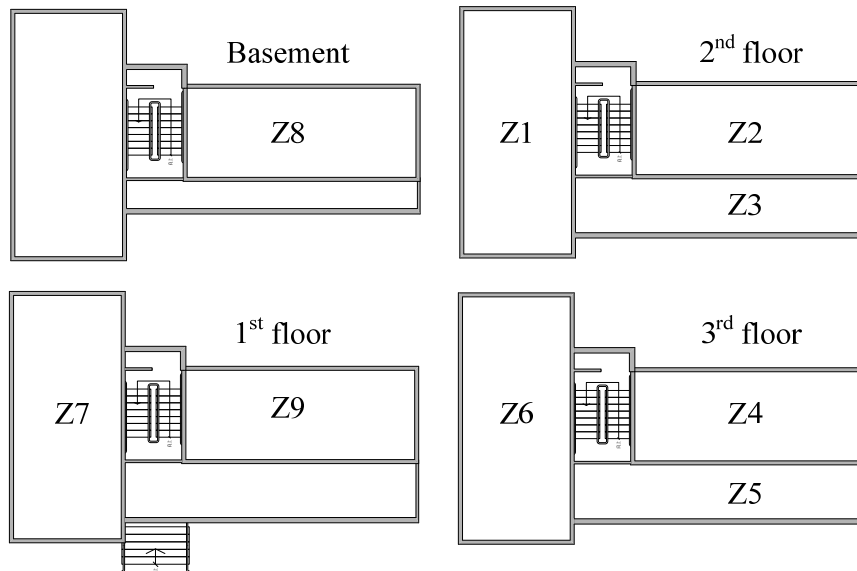


Energy saving assessment-- simulation



Simulation model description:

- 9 zone building with total area of 20,000 sq. ft.
- Data driven envelope model
- Night setup strategy and assume perfect setpoint tracking
- Simulate for a 100-day cooling season with TMY2 data

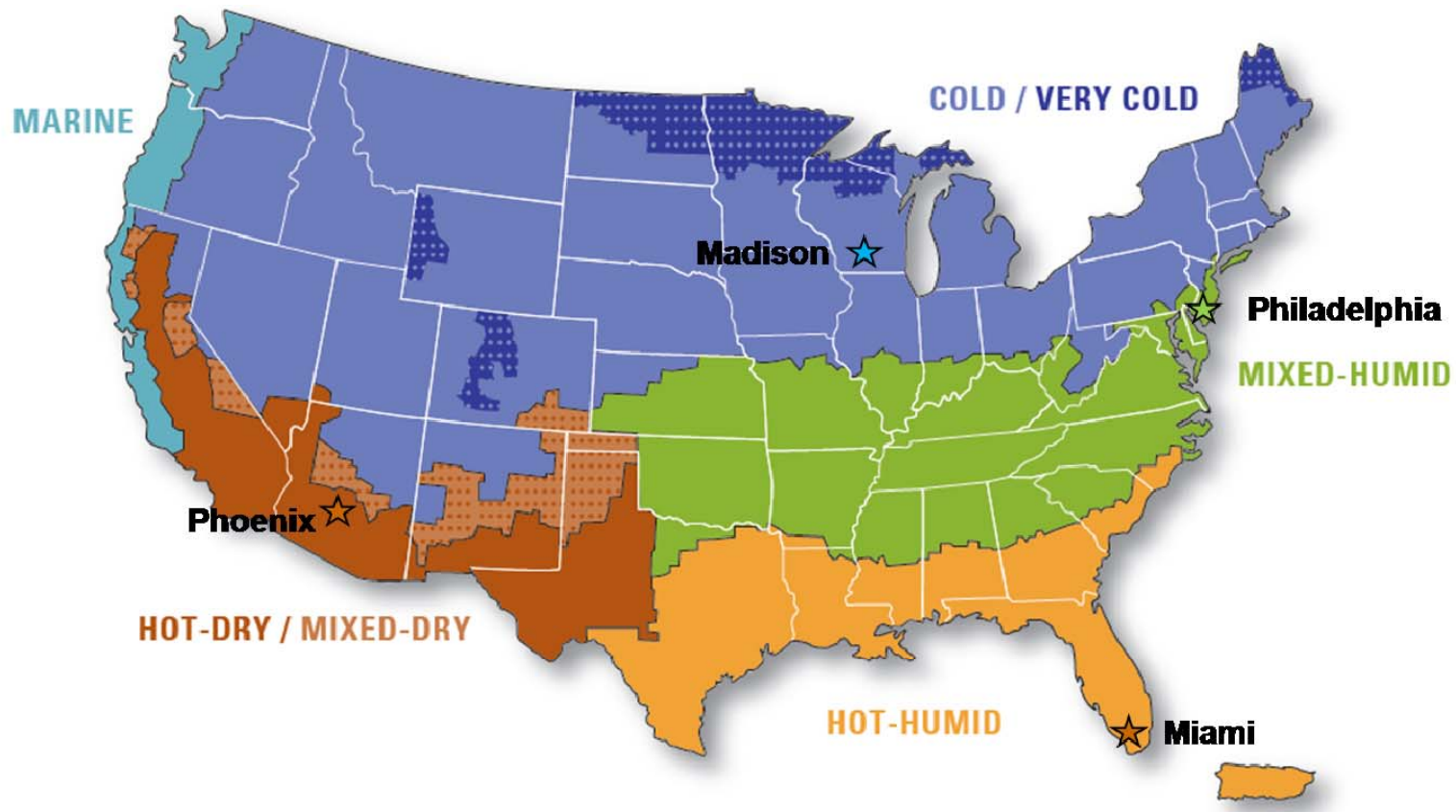




Climate zones for simulation

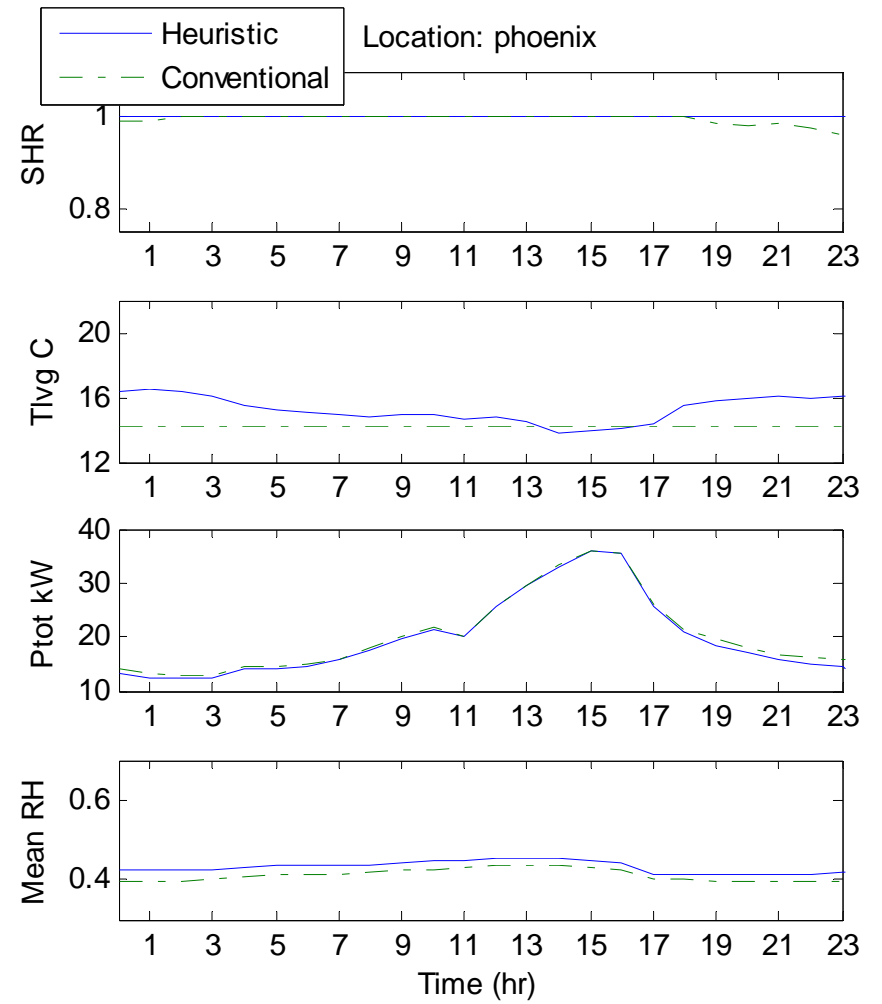
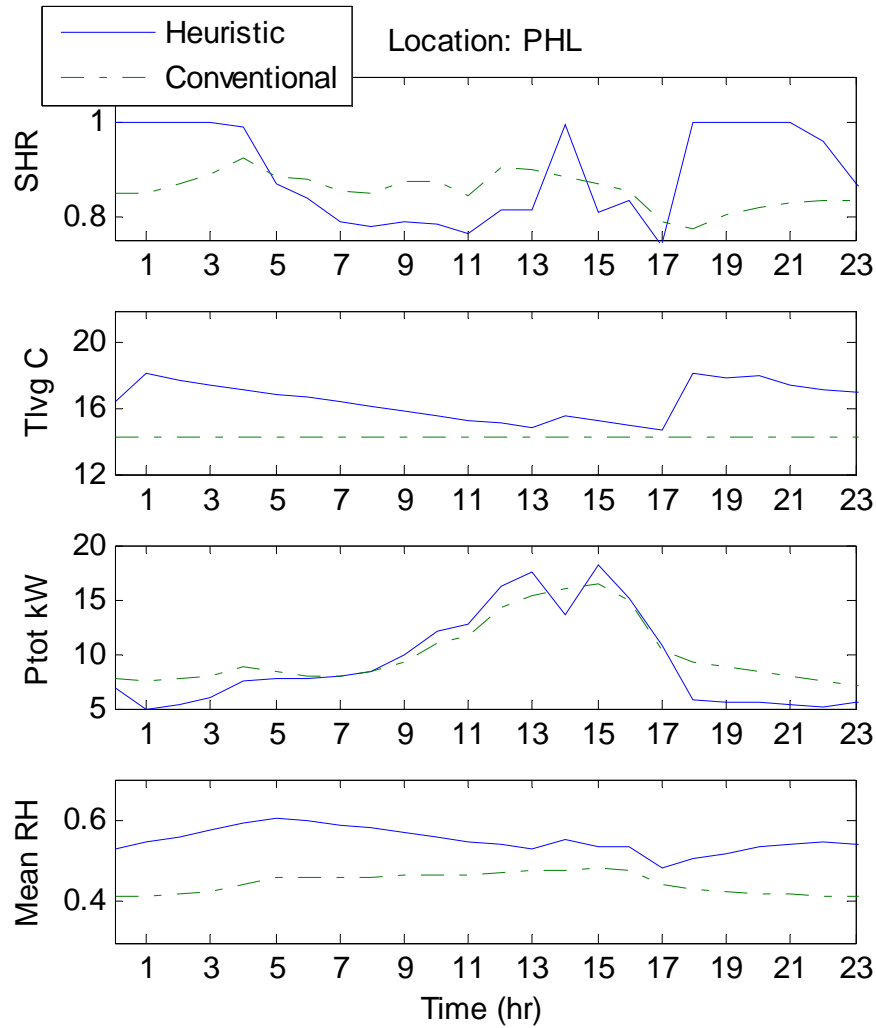


- Four cities are chosen to represent different climates
- DX unit is scaled according to the peak load





Simulation results





Simulation results



Simulation results:

	Qsen on DX coil (MWh)		Qlatent on DX coil (MWh)		Energy consumption (MWh)			Mean zone RH %	
	Heur.	Conv.	Heur.	Conv.	Heur.	Conv.	Saving	Heur.	Conv.
Philadelphia	130.1	130.4	15	17.5	25.8	27.5	8.5 %	53	45
Miami	143	142.6	31.1	31.4	35.5	36.5	2.9%	57	53
Phoenix	173.1	172.7	7.75	11.9	46.5	48.8	4.8%	52	47
Madison	120.5	122.1	8.3	10.5	22.5	24.8	9.3%	55	48

* Comfort improves in addition to energy savings (not listed in the table)



Conclusion



- Variable speed compressor provides better part-load performance than digital scroll compressor in a DX unit
- For both types of compressor, peak efficiency occurs when the coil condition changes from wet to dry
- *Control heuristics*: increase T_{sup} until a SHR upper bound is reached
- The proposed heuristics provide near-optimal control at any operating condition
- Heuristics leads to more energy savings for systems equipped with variable speed compressor and under constant pressure control
- Significant energy savings can be achieved for a whole cooling season, but is highly dependent on the climate



Thank you!

Q&A