# Purdue University Purdue e-Pubs

International Refrigeration and Air Conditioning Conference

School of Mechanical Engineering

1996

# Thermodynamic Properties of Difluoromethane on the Saturation Curve

Y. Chernyak University of Delaware

P. Zhelezny Odessa State Academy of Refrigeration

M. Paulaitis University of Delaware

Follow this and additional works at: http://docs.lib.purdue.edu/iracc

Chernyak, Y.; Zhelezny, P.; and Paulaitis, M., "Thermodynamic Properties of Difluoromethane on the Saturation Curve" (1996). *International Refrigeration and Air Conditioning Conference*. Paper 361. http://docs.lib.purdue.edu/iracc/361

This document has been made available through Purdue e-Pubs, a service of the Purdue University Libraries. Please contact epubs@purdue.edu for additional information.

Complete proceedings may be acquired in print and on CD-ROM directly from the Ray W. Herrick Laboratories at https://engineering.purdue.edu/ Herrick/Events/orderlit.html

# THERMODYNAMIC PROPERTIES OF DIFLUOROMETHANE ON THE SATURATION CURVE

Y. Chernyak\*, P. Zhelezny\*\* and M. Paulaitis\*<sup>†</sup>

 \* Center for Molecular and Engineering Thermodynamics Department of Chemical Engineering, University of Delaware, Newark, DE 19716, USA
 <sup>†</sup> Current Address: Department of Chemical Engineering, Johns Hopkins University, Baltimore, MD 21218, USA

> \*\* Odessa State Academy of Refrigeration Petra Velikogo 1/3, Odessa, 270057, Ukraine

## ABSTRACT

Vapor pressures in the range of 256 to 331 K and saturated liquid and vapor densities from 315 to 331 K have been measured for difluoromethane (HFC-32) on the saturation line by means of variable volume and static experimental methods. Our results have been combined with literature values, and on the basis of all the measurements, accurate analytical correlations for saturated liquid and vapor densities and vapor pressures have been established. The functional form of the correlations is accurate over a wide range of temperatures including those near the critical temperature. The uncertainty in these correlations are comparable to uncertainties in the experimental data on which the correlations are based. Comparisons of thermodynamic properties on the saturated line, calculated using these correlations, with generalized correlations for HFC-32 reported earlier are also discussed.

# INTRODUCTION

Hydrofluorocarbon (HFC) compounds have received much attention as replacement working fluids for refrigeration processes due to their low ozone depletion and global warming potentials. HFC refrigerants are also attractive because of their higher energy efficiency, which reduces of their total global warming impact. However, no single HFC compound has been identified as a replacement for the widely used refrigerants, HCFC-22 and R-502 [1,2]. Alternatively, a number of binary and ternary mixtures containing HFC-32 as a constituent have been identified as potential replacements. Pure difluoromethane is not a feasible working fluid because of its high flammability and vapor pressure, but this HFC can form azeotropic and near-azeotropic mixtures with other compounds and has a higher efficiency than most other alternatives. Therefore, HFC-32 as an added constituent will improve the energy efficiency of refrigerant blends. In the present paper, we combine our measurements of vapor-liquid equilibrium (VLE) for HFC-difluoromethane with data available in the literature to provide thermodynamic properties for this HFC over a wide range of temperatures, induding those in the vicinity of the critical point.

# EXPERIMENTAL RESULTS

Two different experiments have been used to measure the thermodynamic properties of difluoromethane at saturation. A static method was applied to measure vapor pressures. In this method, a 75 cm<sup>3</sup> stainless steel cell was immersed in a Neslab temperature bath which controls temperature to 0.01 K. The temperature of the bath was measured to the same accuracy using a resistance thermometer. The equilibrium cell was connected by stainless steel tubing to one side of a Ruska differential pressure cell (Model 2413-705). The vapor pressure on this side of the differential cell was balanced by nitrogen pressure using a Ruska differential pressure null indicator (Model 2416-711). Nitrogen pressure was controlled and measured to an accuracy of 0.001 MPa with a Heise Precision pressure controller (Model PPC-159). The differential pressure cell, connecting lines, and valves were heated to at least 5 K higher than the bath temperature to ensure no condensation of the vapor phase. Further details of the apparatus and experimental technique are given elsewhere [3].

Vapor pressures have been measured at thirty-two temperatures between 255.95 and 291.21 K. Experimental uncertainties in the temperature are less than  $\pm 0.02$  K, and the maximum uncertainty in pressure is less than 0.2% of the measured value at the lowest pressure. The purity of the sample was 99.95%. The measured vapor pressures are summarized in Table 1.

the second s	1				-		
<i>T</i> , K	P, MPa	<i>T</i> , K	P, MPa	<i>T</i> , K	P, MPa	<i>T</i> , K	P, MPa
255.95	0.4512	259.81	0.5193	267.74	0.6824	280.47	1.0230
255.98	0.4514	261.18	0.5447	268.17	0.6923	281.13	1.0436
256.02	0.4529	263.69	0.5942	270.14	0.7387	282.91	1.1006
256.04	0.4532	264.42	0.6100	270.59	0.7500	285.42	1.1851
256.13	0.4548	265.21	0.6267	272.60	0.8025	285.97	1.2045
256.17	0.4550	265.82	0.6397	273.26	0.8176	287.89	1.2734
256.62	0.4625	266.12	0.6462	275.89	0.8884	289.21	1.3221
258.96	0.5034	267.47	0.6762	279.01	0.9784	291.21	1.3988

Table 1. Experimental vapor pressures of difluoromethane

Vapor pressures, and saturated liquid and vapor densities of difluoromethane have been also measured using a variable volume apparatus with a molibden-glass view cell. This apparatus and the experimental technique have been reported earlier [4] and discussed in detail elsewhere [5]. The measured properties of difluoromethane (99.80% pure) at saturation is given in Table 2 for temperatures between 280.15 and 331.14 K.

Table 2. Experimental vapor pressure, saturated liquid and vapor densities of difluoromethane

<i>T</i> , K	P, MPa	$\rho', \text{kg m}^{-3}$	ρ'', kg m <sup>-3</sup>
280.15	1.0086	-	
298.03	1.6782	-	<u> </u>
315.02	2.5795	884.9	76.6
323.14	3.1331	841.1	97.7
331.14	3.7525	791.0	125.8

Experimental uncertainties in the temperature was estimated to be  $\pm 0.015$  K. The experimental uncertainties in pressure was 0.1 - 0.2%, liquid density - 0.15 - 0.25\%, vapor density - 0.25 - 0.35\%.

# DATA SOURSES AND CALCULATIONS

Table 3 list the saturation conditions and the number of data points that were used in the correlating the thermodynamic properties of difluoromethane.

Table 3, St	ummarv of	experimental	data used	in the	correlations	for	difluoromethane
-------------	-----------	--------------	-----------	--------	--------------	-----	-----------------

Authors, year	Ref. number	Number of data points	Temperature range, K	Pressure range, MPa	Density range, kgm <sup>-3</sup>
	• <u> </u>	Vapor pr	essure	•	
Malbrunot et al., 1968	6	30	191-351	0.016-5.83	-
Adams and Stein, 1971	7	4	222-283	0.105-1.11	-
Kapungo et al., 1987	8	11	149-245	0.0003-0.29	-
Baroncini et al., 1993	9	56	238-351	0.22-5.75	-
Weber and Goodwin, 1993	10	27	208-237	0.049-0.21	-
Widiatmo et al., 1994	11	25	220-325	0.095-3.28	-
Bouchot and Richon, 1994	12	8	253-334	0.4-3.95	-
Türk et al., 1994	13	27	204-351	0.04-5.83	
Fukushima et al., 1995	14	57	277-351	0.93-5.74	_
Oguchi et al., 1995	15	16	243-351	0.27-5.75	-
This work*	-	5	280-331	1.01-3.75	-
This work**		32	256-291	0.45-1.39	-
	<b>.</b>	Saturated liqu	uid density		
Malbrunot et al., 1968	6	15	248-349	-	113-575

Authors, year	Ref. number	Number of data points	Temperature range, K	Pressure range, MPa	Density range, kgm <sup>-3</sup>
Shinsaka et al., 1985	16	20	150-222	- "	1204-1385
Widiatmo et al., 1994	11	22	220-322	-	797-1209
Sato et al., 1994	17	2	321-344	-	675-850
Oguchi et al., 1995	15	5	255-293	-	981-1115
This work*	-	3	315-331	-	791-885
		Saturated var	or density		· · · · ·
Bouchot and Richon, 1994	12	4	253-313	-	11-73
Fukushima et al., 1995	14	5	310-336	-	67-151
This work*	-	3	315-331	-	78-126

\* - Obtained by variable volume method.

\*\* - Obtained by static method.

The functional forms chosen for fitting the vapor pressures, and the saturated liquid and vapor densities [18] are, respectively,

$$\ln(P_c / P_s) = a \ln(T_c / T) + b \left(\ln(T_c / T)\right)^c \tag{1}$$

$$\ln(\rho' / \rho_c) = B_1 \left( \ln(T_c / T) \right)^{\beta F_1(\tau)}$$
(2)

$$\ln(\rho_{\rm c} / \rho'') = B_2 (\ln(T_{\rm c} / T))^{\beta F_2(\tau)}$$
(3)

where  $\tau = \ln(T_c/T)$ ; *a*, *b*, *c*, *B*<sub>1</sub>, *B*<sub>2</sub>,  $\beta$  are the fitted coefficients, which depend on the specific properties of diffuoromethane; and  $F_1(\tau)$ ,  $F_2(\tau)$  are the following universal crossover functions,

$$F_{1}(\tau) = 1 - 1.113 \tau^{0.4} / \ln \tau \tag{4}$$

$$F_2(\tau) = 1 + 4.82\tau^{0.6} / \ln \tau \tag{5}$$

The critical parameters for difluoromethane used in Eqs. (1) - (3) were determined on the basis of data reported in the literature (Table 4). Initially, we determined average values of the critical parameters weighted by their standard deviations and values for the average standard deviation using the data in Table 4. These parameters were then used in Eqs. (1) - (3) to obtain an optimal set of critical parameters using the data from this work. The critical properties for difluoromethane that were used in the present calculations and the coefficients in Eqs. (1) - (3) are given in Table 5.

Table 4. Summary of critical properties measurements for difluoromethane

Authors, year	Ref. number	Critical temperature, K	Critical density, kg m <sup>-3</sup>	Critical pressure, MPa	Purity,
Malbrunot et al, 1968	6	351.54±0.2	430	5.830	99.85
Smith and Srivastava, 1986	19	351.0	-	-	
Singh et al., 1991	20	351.56±0.02	429.61	5.814	
Nishimura et al., 1992	21	- 1	-	5.780±0.002	99.98
Fukushima and Ohotoshi, 1993	22	351.26±0.03	425+5	5778+0.003	99.98
Holcomb et al., 1993	23	-	428.50±1.83	-	99.9
Jelinek and Daltrophe, 1993	24	351.55	429.6		-
Grebenkov, 1993	25	351.55	421.1	5.843	
Schmidt and Moldover, 1994	26	351.36±0.02	419±7	5.7927±0.024	99.9

Authors, year	Ref.	Critical temperature,	Critical density,	Critical pressure,	Purity,
-	number	ĸ	kg m <sup>-3</sup>	MPa	%
Higashi, 1994	27	351.26±0.01	427±5	5.785±0.009	99.98
Kuwabara et al., 1994	28	351.255±0.01	424±1	-	99.9 <u>9</u> 8
Sato et al., 1994	16	-	-	5.784±0.0025	99.9
Türk et al., 1994	14	351.23±0.06	420±8	5.783±0.06	99.98

Table 5. Critical properties and coefficients in Eqs. (1) - (3)

<i>T</i> <sub>c</sub> , K	351.255		
P <sub>c</sub> , MPa	5.784		
$\rho_c$ , kg m <sup>-3</sup>	424		
a	7.26622		
b	5.53976		
с	2.686		
β	0.32475		
<i>B</i> <sub>1</sub>	1.75095		
<i>B</i> <sub>2</sub>	2.30530		

### DISCUSSION

Deviations of the calculated properties using Eqs. (1) - (3) from the experimental data (Table 3) do not exceed 0.5% for vapor pressure, 0.4% for saturated liquid and 1.3% for saturated vapor density over entire range of temperatures investigated.

Eqs. (1) - (3) are also in satisfactory agreement with other correlations reported earlier [29, 30] as shown by the comparisons in Figs. 1, 2, and 4. Deviations in vapor pressures (Fig. 4) over the temperature range from 250 K to the critical temperature is less than 1%. Similar systematic deviations in vapor pressure at low temperatures are due to experimental data used to develop the vapor pressure correlation [29, 30], which did not include data by Malbrunot et al. [6] and Kanungo [8] at temperature from 191 to 350 K and 149 to 245 K, respectively.

The present calculations of saturated liquid density are in a good agreement with previous calculations [29, 30] at all temperatures except near the critical point (Fig. 2). In these previous works, multiple-term scaling-type equations for saturated liquid density were chosen. It should be noted that the critical index,  $\beta$ , used in [29] and [30] was 0.355 and 0.3, respectively is much different than the theoretically estimated value of  $\beta=0.3245$  and the value in Table 5 of  $\beta=0.32475$ . In this case, using  $\beta=0.32475$  with a universal crossover function that approaches 1 as the temperature approaches the critical temperature, gives an adequate description of the experimental data over a wide range of conditions including those in a vicinity of the critical point :  $t=1-T/T_{\rm C}<0.1$ .

Taking into account that the liquid density measurements are more reliable and have a higher accuracy than the vapor density measurements, we used the same value of  $\beta$  in Eq.(3) for calculating the vapor densities of difluoromethane. The accurate description of measured liquid and vapor densities using Eqs.(2) and (3), respectively, and their predictive ability in the vicinity of the critical region are shown in Fig. 3 by comparing these calculations with the two independent Wagner-type correlations developed by Kuwabara et al. [28] and Higashi [27] on the basis of their own data near the critical point. In spite of the fact that experimental data in the critical region was not included in developing our Eqs.(2) and (3) (due to difficulties determining the phase boundary accurately in the vicinity of the critical point), Fig.3 shows very good agreement with the other correlations: within 1.5% for the saturated liquid densities and 2.5% for the saturated vapor densities.

Fig.4 is a plot of deviations in saturated vapor densities of HFC-32 using Eq. (3) by [29] and [30]. In one case [30], the calculated saturation densities were obtained on the basis of an equation of state that had been developed without

the experimental dew point curve. As a result, those results show deviations on the order of 4 - 6% higher that our results at overlapping temperatures. The saturated vapor density data used by Outcalt and McLinden [29] included the data of Defibaugh et al. [31]. The deviations in saturated vapor densities calculated in this case are less than 2% over temperatures from 260 to 350 K, which is less than experimental uncertainties of the data along the saturation curve. Limitations to the application of Eq.(3) are determined by its functional form, which allows describing vapor densities over a the wide range of condition in the critical region, but does not give a smooth transition to an ideal gaseous state at  $T/T_c < 0.65$  and  $\rho < 10-20 \text{ kg m}^{-3}$ .

### CONCLUSION

Basis on measurements of the saturated thermodynamic properties, which includes our own data and experimental results from the literature, accurate correlations for vapor pressure, and saturated liquid and vapor densities of difluoromethane were developed. The functional forms of the correlations are simple, have only a few terms, and allow the prediction of these thermodynamic properties for difluoromethane along the saturation curve over wide temperature range and in the vicinity of the critical point.

### REFERENCES

- 1. Didon, D.A. Bulletin of the IIR (1994), LXXIV, 3, 5.
- 2. Cavallini, A. Proc. 19th Int. Congr. of Refrig. (1995), IVa, 25.
- 3. Chai Kao, C.-P., Paulaitis, M.E., Sweany, G.A. and Yokozeki, A. Fluid Phase Equilibria (1995), 108, 27.
- 4. Zhelezny, V., Chernyak, Y. and Zhelezny, P. Proc. 4th Asian Thepmoph. Prop. Conf. (1995), 2, 291.
- 5. Chernyak, Y. Ph. D. Dissertation, State Academy of Food Technology, Odessa, Ukraine (1994).
- 6. Malbrunot, P.E., Meunier, P.A., Scatena, G.M., et al. J. Chem. Eng. Data (1968), 13, 16.
- 7. Adams, R.A. and Stein, F.P. J. Chem. Eng. Data (1971), 6, 146.
- 8. Kanungo, A., Takao, O., Popowicz, A. and Ishida, T. J. Phys. Chem. (1987), 91, 4198.
- 9. Baroncini, C., Camporese, R., Giuliani, G., et al. High Temp. High Pres. (1993), 25, 459.
- 10. Weber, L.A. and Goodwin, A.R.H. J. Chem. Eng. Data (1993), 38, 254.
- 11. Widiatmo, J.V., Sato, H. and Watanabe, K. J. Chem. Eng. Data (1994), 39, 304.
- 12. Bouchot, C. and Richon, D. Proc. Int. Conf. "CFCs, the day after", Padova, Italy (1994), 517.
- 13. Türk, M., Zhai, J., Nagel, M. and Bier, K. Fortschr.-Ber. VDI Reihe 19, Nr.79, Düsseldorf, VDI-Verlag (1994).
- 14. Fukushima, M., Ohotoshi, S. and Miki, T. Proc. 19th Int. Congr. of Refrig. (1995), IVa, 207.
- 15. Oquchi, K., Takaishi, Y., Yada, N., Namiki, T. and Sato, T. Proc. IEA Annex 18 meeting, Gothenburg, MD (1995)
- 16. Shinsaka, K., Gee, M. and Freeman, G.R. J. Chem. Thermodyn. (1985), 47, 1111.
- 17. Sato, T., Sato, H. and Watanabe, K. J. Chem. Eng. Data (1994), 39, 851.
- Zhelezny, V.P., Kachurka, Y.A., Lyasota, L.D. and Semenyuk, Y.V. Proc. VIII All-Union Conf. on Thermoph. Prop. Novosibirsk, USSR (1988), 31.
- 19. Smith, B.D. and Srivastava, R. Phys. Sci. Data (1986), 25.
- 20. Singh, R.R., Lund, E.A.E. and Shankland, I.R. Proc. CFC and Halon Int. Conf. Baltimore, MD (1991), 451.
- 21. Nishimura, A., Qian, Z., Sato, H. and Watanabe, K. Proc. 13th Japan Thermoph. Prop. Symp., Akita, Japan (1992), 57.
- 22. Fukushima, M. and Ohotoshi, S. Proc. 27th Japan Joint Conf. Air-cond. Refrig., Tokyo, Japan (1993), 173.
- 23. Holcomb, C.D., Niesen, V.G., Van Poolen, L.J. and Outcalt, S.L. Fluid Phase Equilibria (1993), 91, 145.
- 24. Jelinek, M. and Daltophe, N.C. Proc. Int. Conf. "Energy efficiency in refrigeration and global warming impact", Belgium (1993) 298.
- 25. Grebenkov, A.J. Private communication (1993).
- 26. Schmidt, J.W. and Moldover, M.R. J. Chem. Eng. Data (1994), 39, 39.
- 27. Hihashi, Y. Int. J. Refrig. (1994), 17, 524.
- 28. Kuwabara, S., Sato, H, and Watanabe K. High Temp.-High Pres. (1994), 26, 35.
- 29. Outcalt, S.P. and McLinden, M.O. Proc. 12th Symp. on Thermoph. Prop., Boulder, CO (1994), 73.
- 30. Japanese Association of Refrigeration Thermodynamic Tables. Vol. 1., HFCs and HCFCs, Tokyo, Japan (1994).
- 31. Defibaugh, D.R., Morrison, G. and Weber, L. J. Chem. Eng. Data (1994), 33, 333.



Fig.1 Deviation of vapor pressure of HFC-32 from Eq.(1)



Fig.2 Deviation of saturated liquid densities of HFC-32 from Eq.(2)



Fig.3 Deviation of saturated liquid and vapor densities of HFC-32 from Eqs.(2) and (3)



Fig.4 Deviation of saturated vapor densities of HFC-32 from Eq.(3)