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The Use of a Four-Microphone Standing Wave Tube to Estimate the Anisotropic Properties of Fibrous Noise Control Materials

J Stuart Bolton
Purdue University, bolton@purdue.edu

Taewook Yoo

Jonathan H. Alexander
3M Corp.

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The use of a four-microphone standing wave tube to estimate the anisotropic properties of fibrous noise control materials

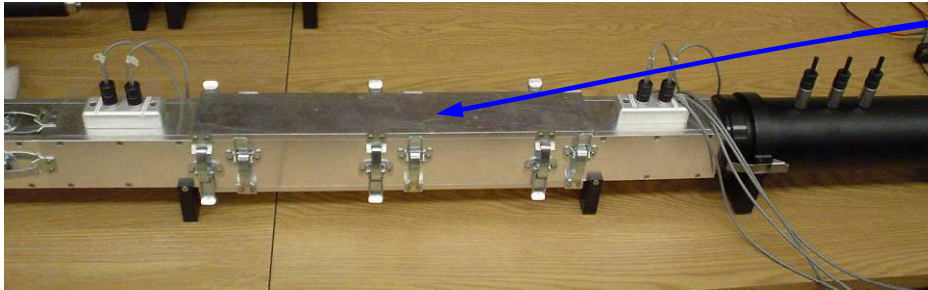
Taewook Yoo

J. Stuart Bolton

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Overall Approach

1. Measuring TL and absorption coefficient in square tube



2. Estimating material properties (COMET/Trim)

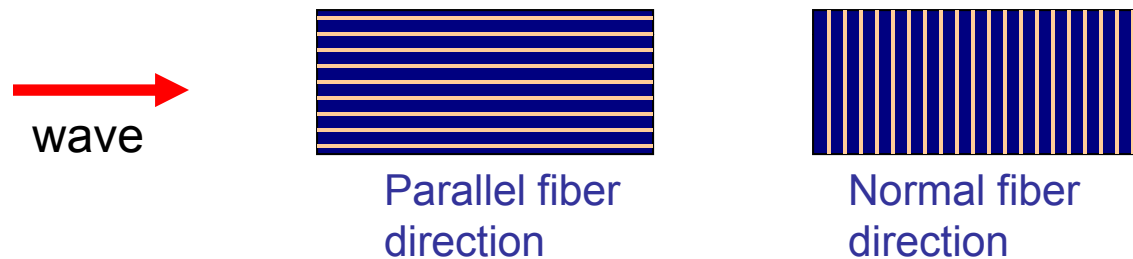
- Flow resistivity, Characteristic lengths, tortuosity, porosity, bulk density, Young's modulus, Poisson's ratio, loss factor

3. Predicting performance using FEM (COMET/SAFE)

- Partially filled cases

Introduction & Objectives

- Fibrous material
 - Blown in certain direction: Thus are anisotropic
 - Level of anisotropy depends on density of fiber, fiber's material and physical dimensions



- Anisotropy
 - Performance differs with respect to wave direction with respect to fiber orientation
 - When is the performance better?
 - Estimation of material properties in different fiber orientations
 - Prediction of performance with the estimated properties

Material Properties I

- **Nine properties** represent a material
 1. Flow resistivity
 - Pressure drop from low velocity flow in material
 - One of the most sensitive properties to performance
 2. Viscous characteristic length
 - Depth of viscous boundary layer
 - Sensitive properties
 - Range: $1 \times 10^{-5} \sim 9.99 \times 10^{-4}$ m
 3. Thermal characteristic length
 - Depth of thermal boundary layer
 - Sensitive properties
 - Range: $1 \times 10^{-5} \sim 9.99 \times 10^{-4}$ m

Material properties II

4. Tortuosity

- Complexity in structure (usually 1.1 for fibrous material)

5. Porosity

- Ratio of open to closed volume in bulk material
- Usually 0.99 for fibrous material

6. Bulk density

- Weight per unit volume

7. Young's modulus

- Axial stiffness of bulk material (usually less than 20 kPa for fibrous media)

8. Poisson's ratio

- Ratio of change in dimension in two different directions

9. Loss factor

- Energy dissipation in solid material

Materials



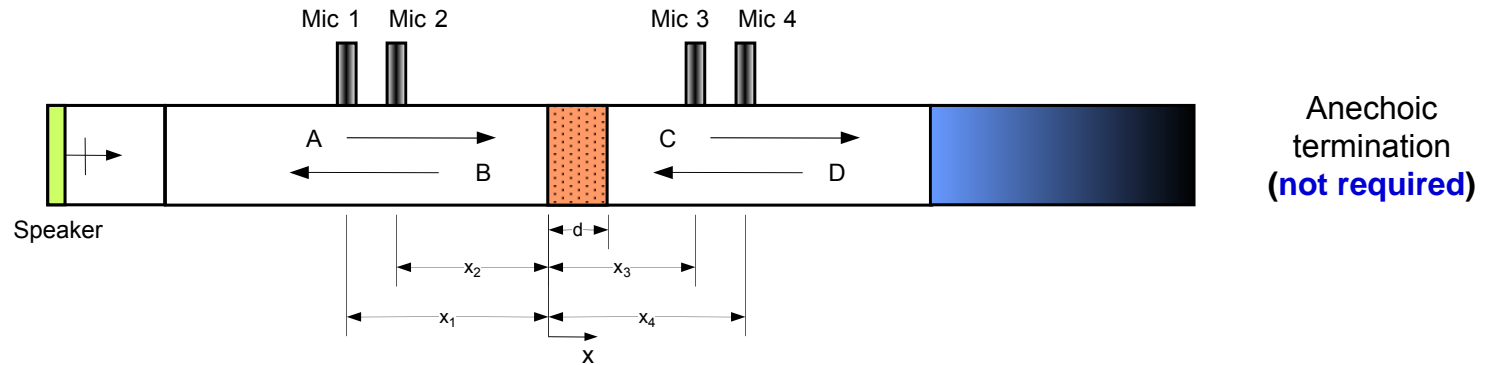
THL



TC

	THL	TC
Thickness [cm]	3.7	4
Mass per unit area [g/m ²]	156	376
Material	Polyester	Polypropylene + Polyester
Fiber size	Normal	Fine

Measurements of TL – square or round



1. Measuring sound pressure:

$$P_1 = (Ae^{-jkx_1} + Be^{jkx_1})e^{j\omega t} \quad P_3 = (Ce^{-jkx_3} + De^{jkx_3})e^{j\omega t}$$

$$P_2 = (Ae^{-jkx_2} + Be^{jkx_2})e^{j\omega t} \quad P_4 = (Ce^{-jkx_4} + De^{jkx_4})e^{j\omega t}$$

2. Calculate complex amplitude of waves:

$$A = \frac{j(P_1e^{jkx_2} - P_2e^{jkx_1})}{2 \sin k(x_1 - x_2)} \quad C = \frac{j(P_3e^{jkx_4} - P_4e^{jkx_3})}{2 \sin k(x_3 - x_4)}$$

$$B = \frac{j(P_2e^{-jkx_1} - P_1e^{-jkx_2})}{2 \sin k(x_1 - x_2)} \quad D = \frac{j(P_4e^{-jkx_3} - P_3e^{-jkx_4})}{2 \sin k(x_3 - x_4)}$$

* Measurements are averaged over 10 sets of samples

3. Estimate transfer matrix elements:

$$T_{11} = \frac{P|_{x=d} V|_{x=d} + P|_{x=0} V|_{x=0}}{P|_{x=0} V|_{x=d} + P|_{x=d} V|_{x=0}} \quad T_{12} = \frac{P|_{x=0}^2 - P|_{x=d}^2}{P|_{x=0} V|_{x=d} + P|_{x=d} V|_{x=0}}$$

$$T_{21} = \frac{V|_{x=0}^2 - V|_{x=d}^2}{P|_{x=0} V|_{x=d} + P|_{x=d} V|_{x=0}} \quad T_{22} = \frac{P|_{x=d} V|_{x=d} + P|_{x=0} V|_{x=0}}{P|_{x=0} V|_{x=d} + P|_{x=d} V|_{x=0}}$$

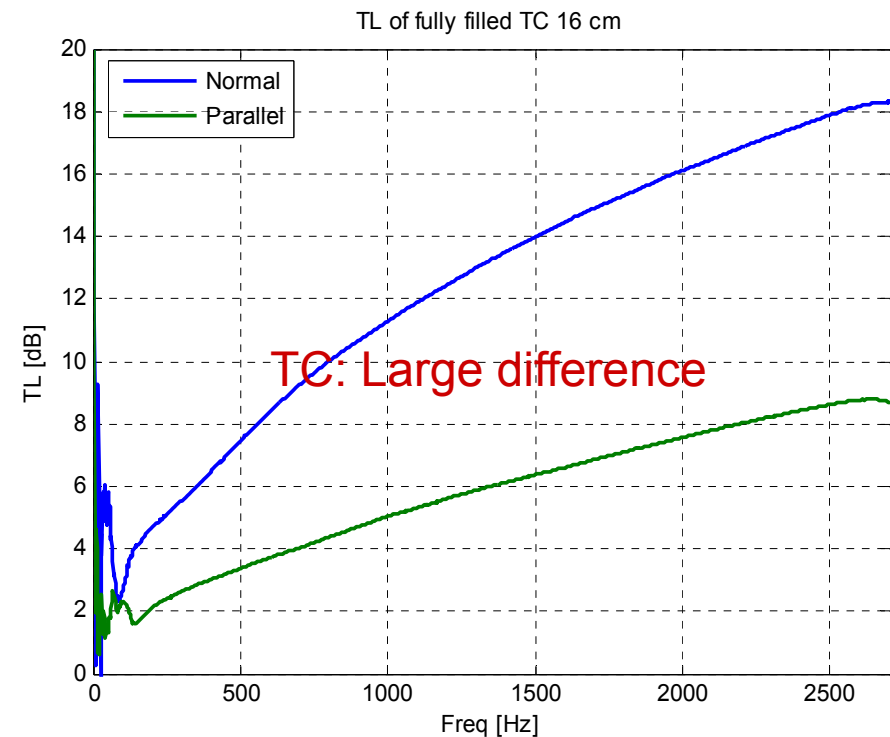
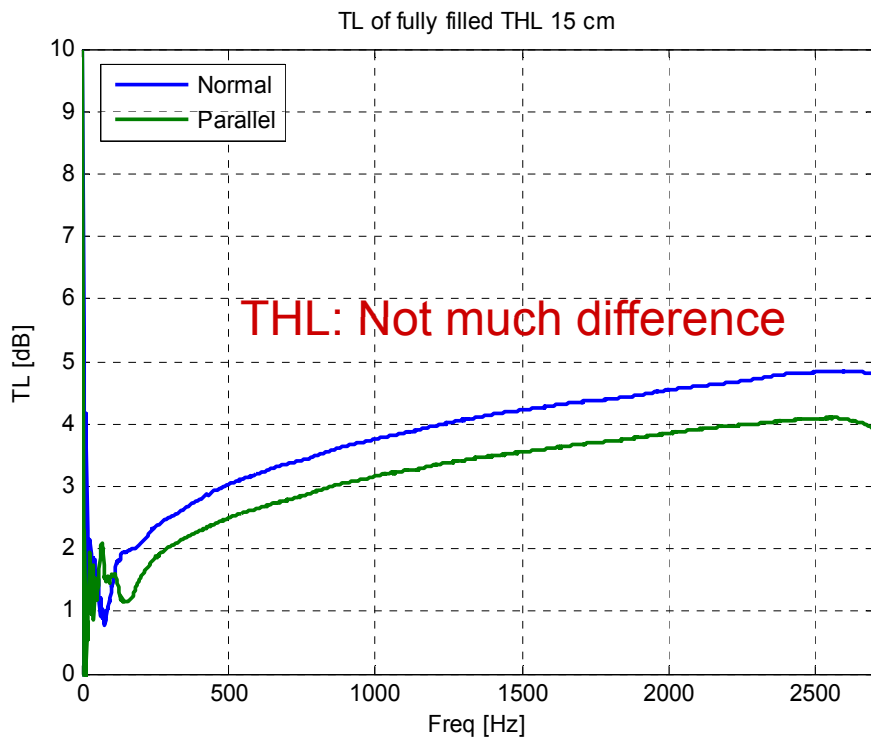
4. Obtain Transmission loss:

$$TL = 20 \log_{10} (1/|T|)$$

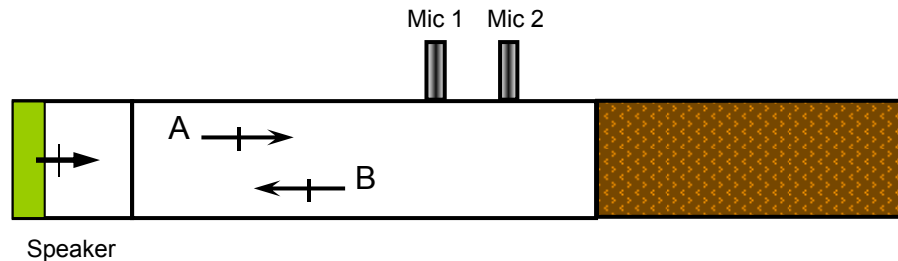
$$\text{Where, } T = \frac{2e^{jkd}}{T_{11} + (T_{12} / \rho_0 c) + \rho_0 c T_{21} + T_{22}}$$

TL's in Two Orientations

- Averaged over ten measurements
 - Normal: using 4 layers
 - Parallel: samples were cut to have same weight as normal cases



Measurement of Absorption coefficient



Normal Incidence
Absorption coefficient

1. Sound pressures

$$P_1 = (Ae^{-jkx_1} + Be^{jkx_1})e^{j\omega t}$$

$$P_2 = (Ae^{-jkx_2} + Be^{jkx_2})e^{j\omega t}$$

2. Measuring transfer function

$$H_{21} = \frac{Ae^{-jkx_2} + Be^{jkx_2}}{Ae^{-jkx_1} + Be^{jkx_1}}$$

$$H_{21} = \frac{e^{-jkx_2} + Re^{jkx_2}}{e^{-jkx_1} + Re^{jkx_1}}$$

3. Solve for R

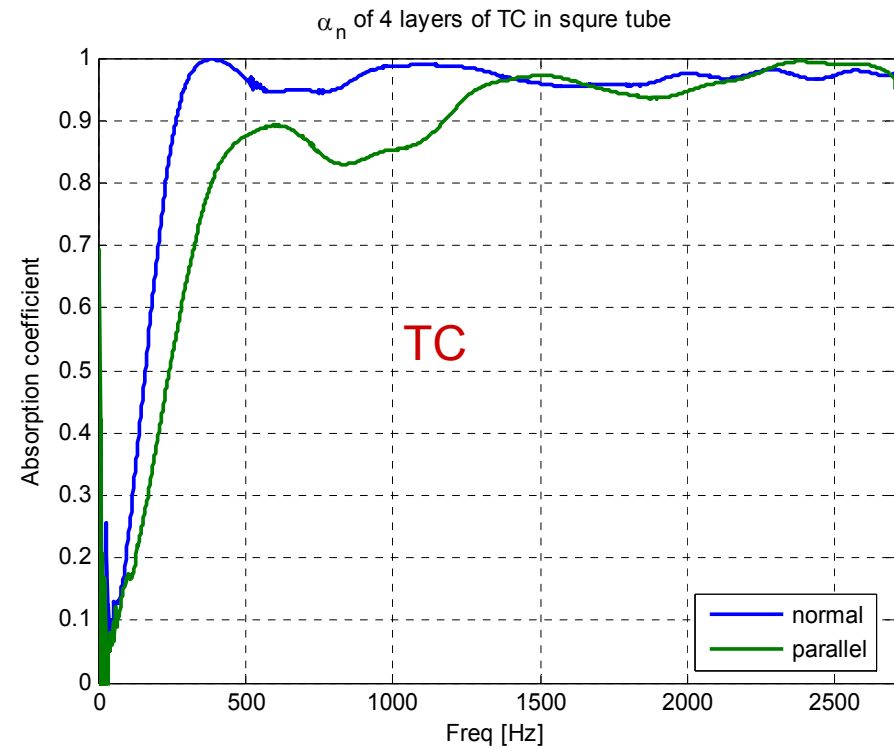
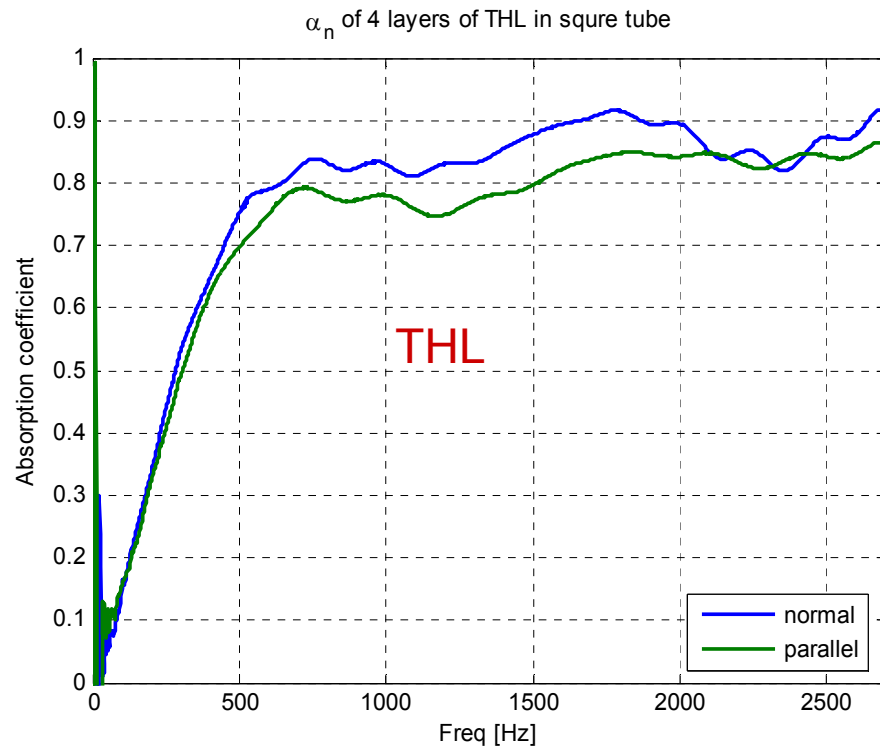
4. Absorption coefficient

$$\alpha = 1 - |R|^2$$

* Measurements are averaged
over 10 sets of samples

Absorptions in Two Orientations

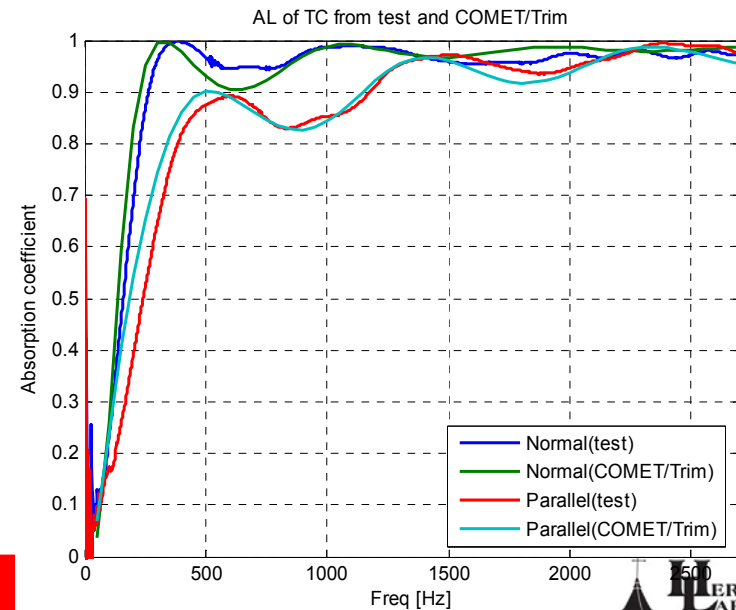
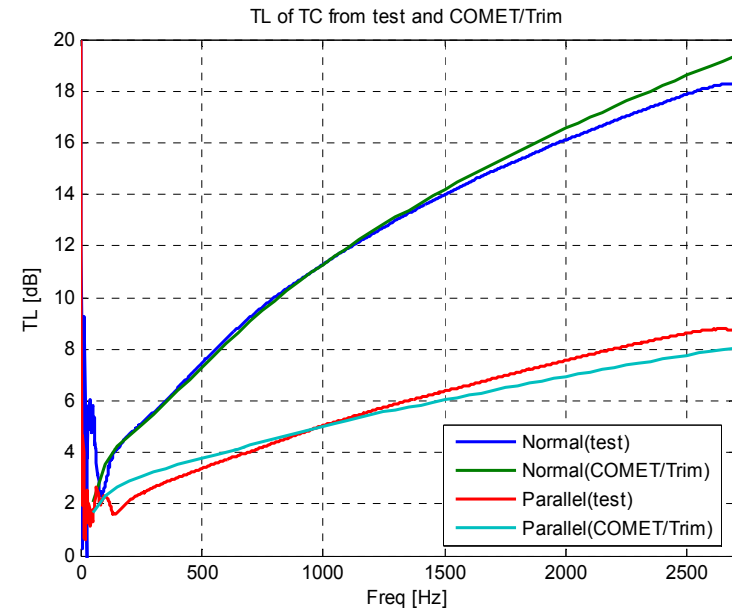
- Averaged over ten measurements
 - Normal: using 4 layers
 - Parallel: samples were cut to have same weight as normal cases



Estimation of TC Properties

Using inverse characterization in COMET/Trim

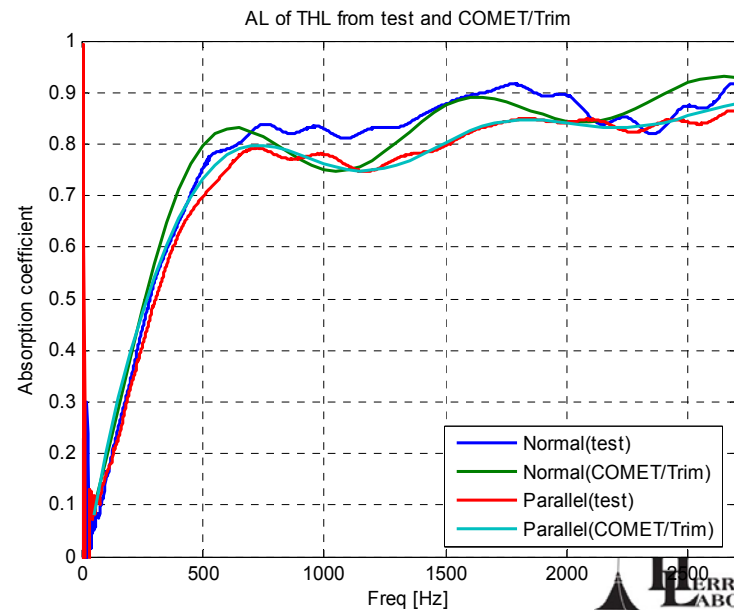
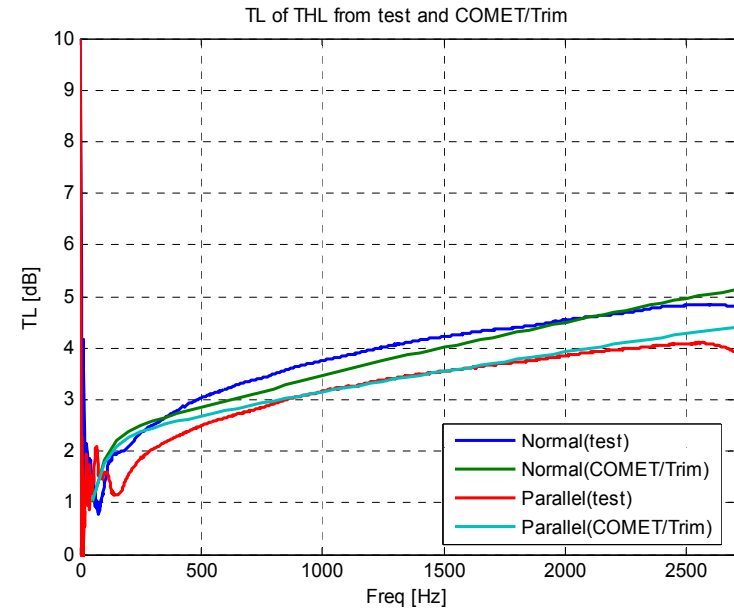
Material	TC	
Fiber direction	Normal	Parallel
Thickness [mm]	40	40
Porosity	0.99	0.99
Flow resistivity [Rayls/m]	5500	1200
Tortuosity	1.1	1.1
Viscous characteristic length [m]	7.90E-05	1.90E-04
Thermal characteristic length [m]	1.52E-04	3.55E-04
Bulk density [kg/m ³]	9.4	9.4
Young's modulus [Pa]	2000	2000
Poisson's ratio	0.3	0.3
Loss factor	0.3	0.3



Estimation of THL Properties

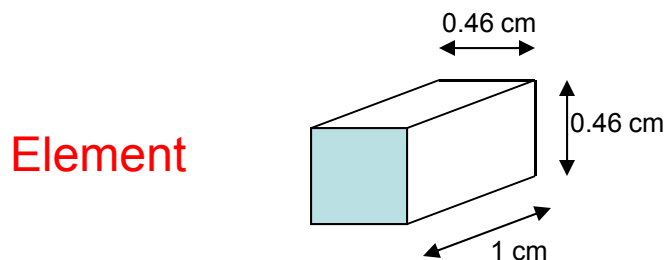
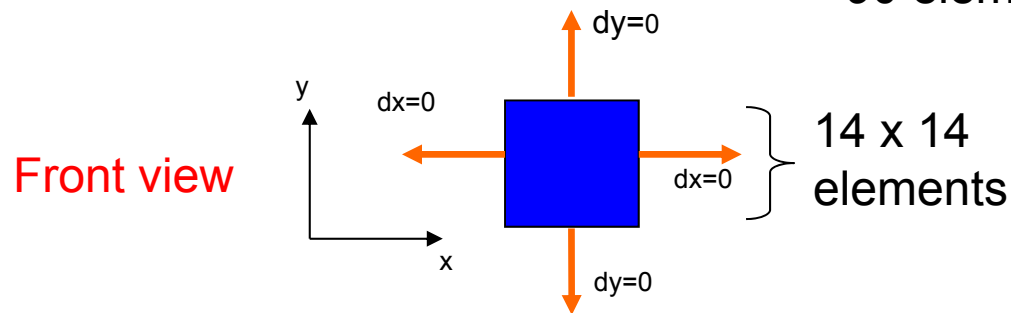
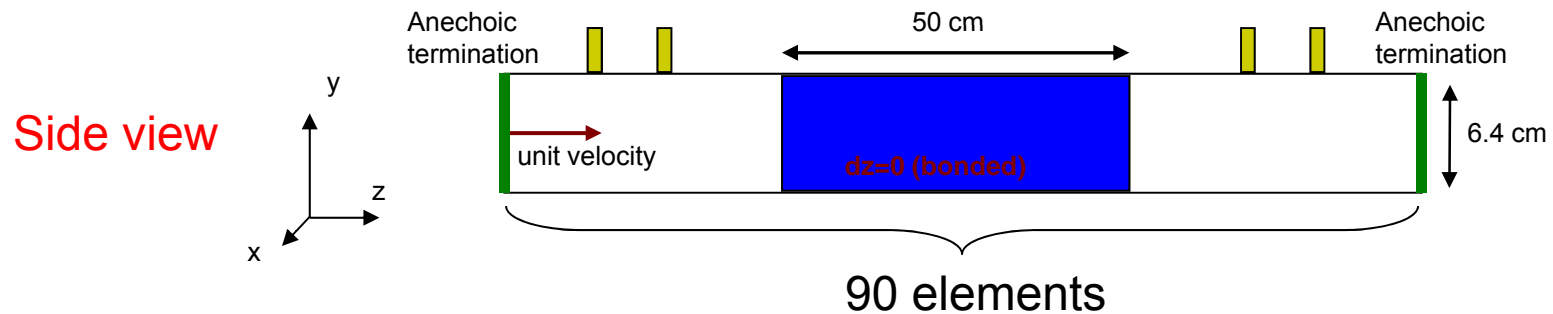
Using inverse characterization in COMET/Trim

Material	THL	
	Normal	Parallel
Fiber direction	Normal	Parallel
Thickness [mm]	37	37
Porosity	0.99	0.99
Flow resistivity [Rayls/m]	2300	1560
Tortuosity	1.1	1.1
Viscous characteristic length [m]	3.00E-04	4.67E-04
Thermal characteristic length [m]	8.29E-04	4.67E-04
Bulk density [kg/m ³]	4.16	4.16
Young's modulus [Pa]	3000	3000
Poisson's ratio	0.3	0.3
Loss factor	0.3	0.3



Finite Element Method

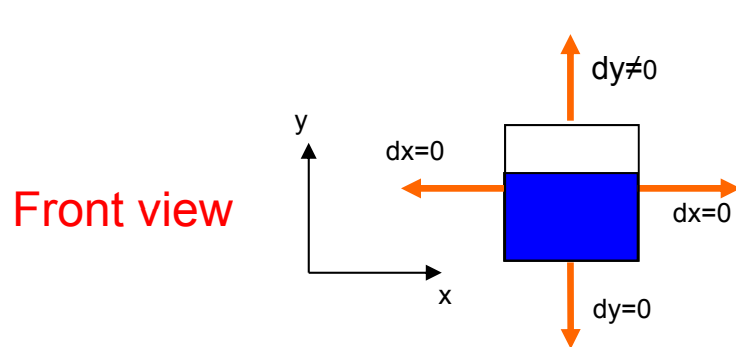
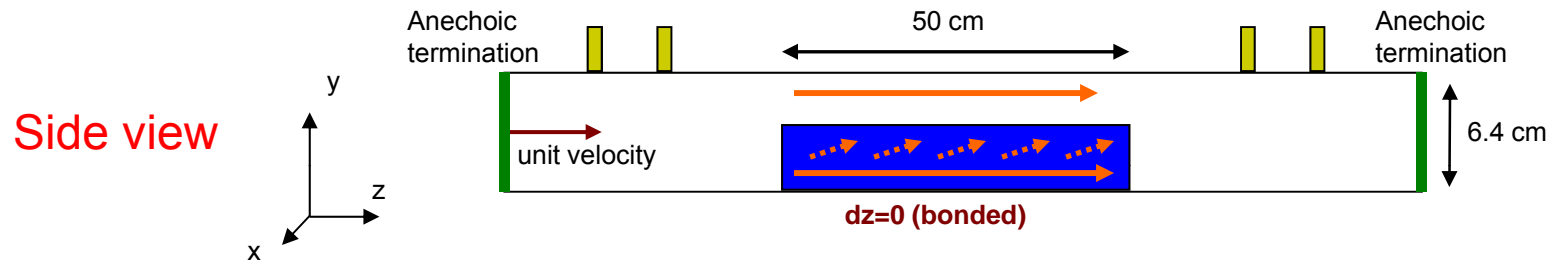
- Dimensions are same as experiment setup



$$\frac{\lambda}{4} = \frac{c}{4 \cdot f} = \frac{340}{4 \cdot 2700} = 0.0315 > 0.01$$

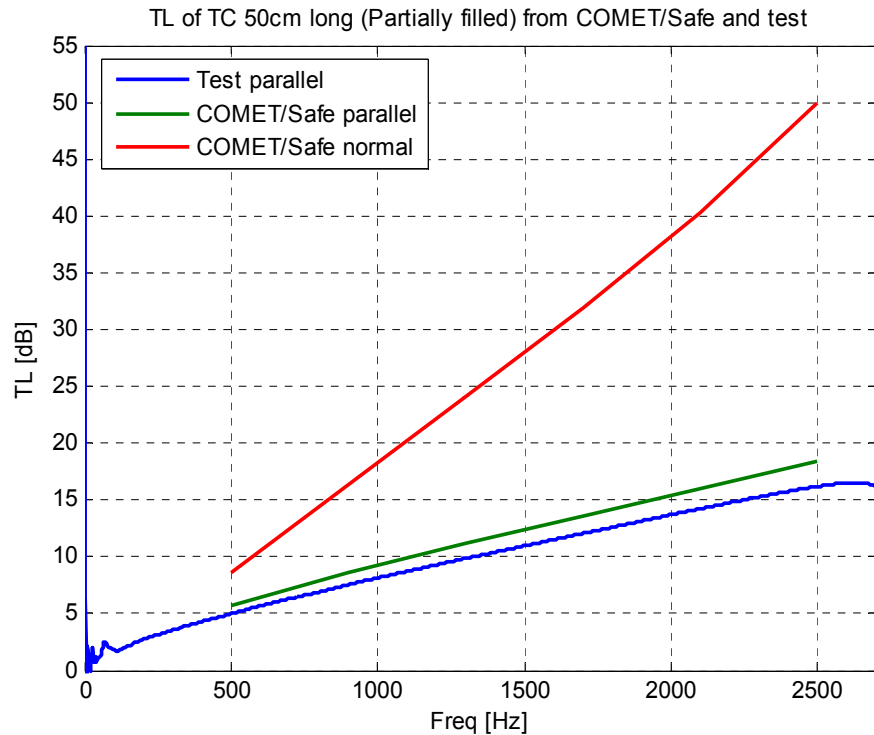
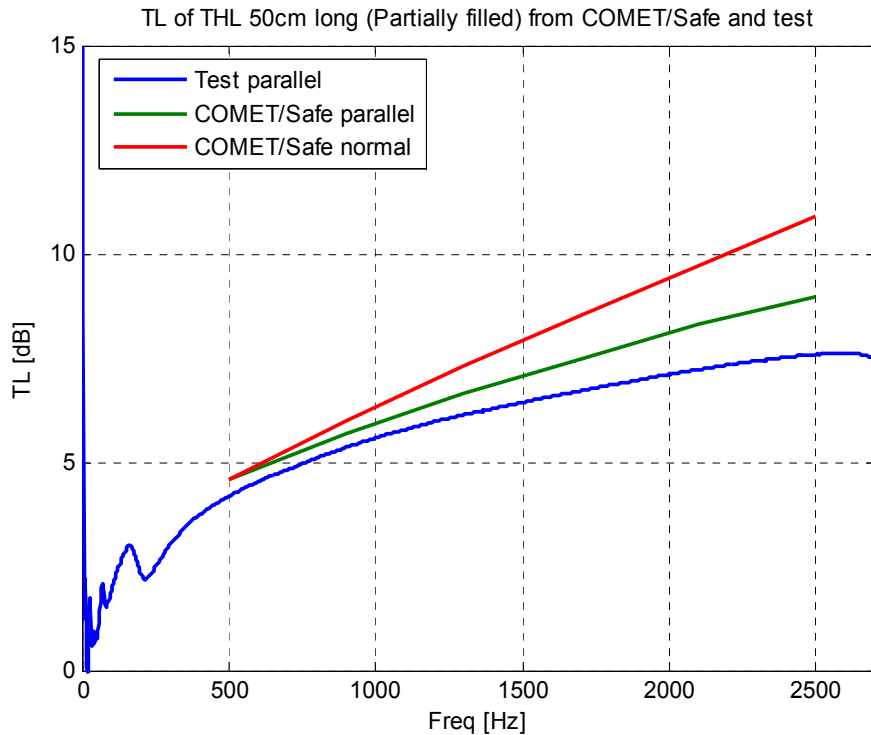
Partially Filled Cases

- Using single layer of TC and THL



- Traveling in empty space
- Traveling inside the material
 - Wave moves in z and y directions
 - Anisotropy affects the results

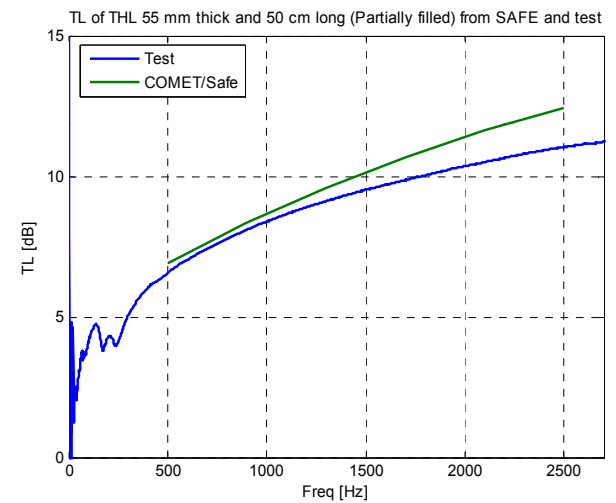
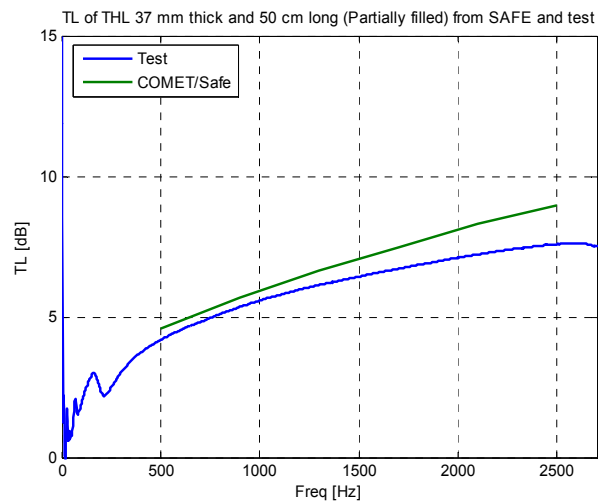
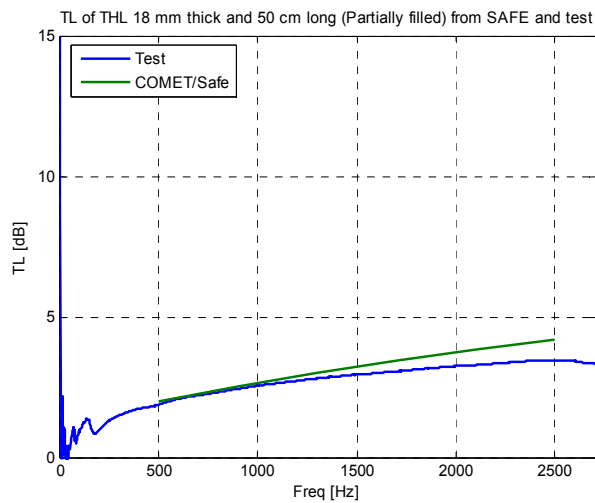
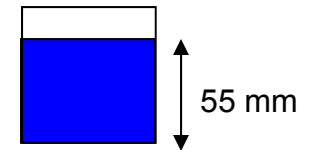
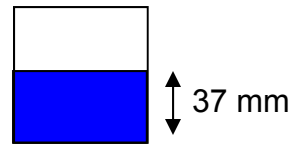
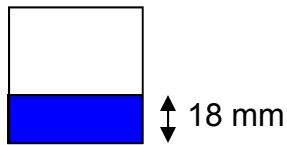
Test and FEM results



Good agreement between test and prediction with both materials

- THL shows a small difference with different fiber orientations
- TC shows large difference with different fiber orientations

Variation in Lining Thickness



- As the sample fills the duct, TL increases
- The prediction and test show good agreement

Conclusions

- There were large differences in performance and in estimated material properties
 - When the fiber orientation was normal to the wave direction, higher flow resistivity. Thus higher transmission loss and absorption were found
 - Depending on fiber orientation, TC material has much larger difference in performance than THL because of finer fiber size and scrims
- Homogeneous model predicts anisotropic materials when proper material properties are used
 - Material properties were successfully estimated
 - Performances in partially filled tube were accurately predicted using finite element model